

# Heat Treatment Principles and Practices

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# Contents

- **Principles of heat treatment of steels**
  - Phase Transformation on heating
  - Forming of austenite
    - Kinetics of formation of austenite
    - Nucleation sites in eutectoid steels
    - Austenitic grain size, Grain growth, Determination of austenitic grain size, Importance of austenitic grain size
- **TTT and CCT diagrams**
  - TTT diagram
    - Method of plotting
    - Types of TTT diagram
    - Critical cooling rate,
    - Effect of alloying elements on TTT diagram, Applications
  - CCT Diagram
    - Continuous cooling transformation diagram
    - Limitations of Iron-Iron Carbide Diagram
    - Effect of Alloying elements on CCT diagram.

# Introduction

- 80% alloys in industrial use are Fe-C alloy
- Purest form of Fe is 99.999% which contain 60 ppm impurities
  - 50ppm – metallic impurities
  - 10ppm – non-metallic impurities (like C, O, S, P)

# Allotropy of Fe

Metals which exhibits more than one crystal structure depending on the temperature & or Pressure – **Allotropy**

**Example :**

**Ti & Zr**

HCP → BCC at 882 & 815°C respectively

**Sn**

cubic(grey) → Tetragonal(white) at 13.2°C

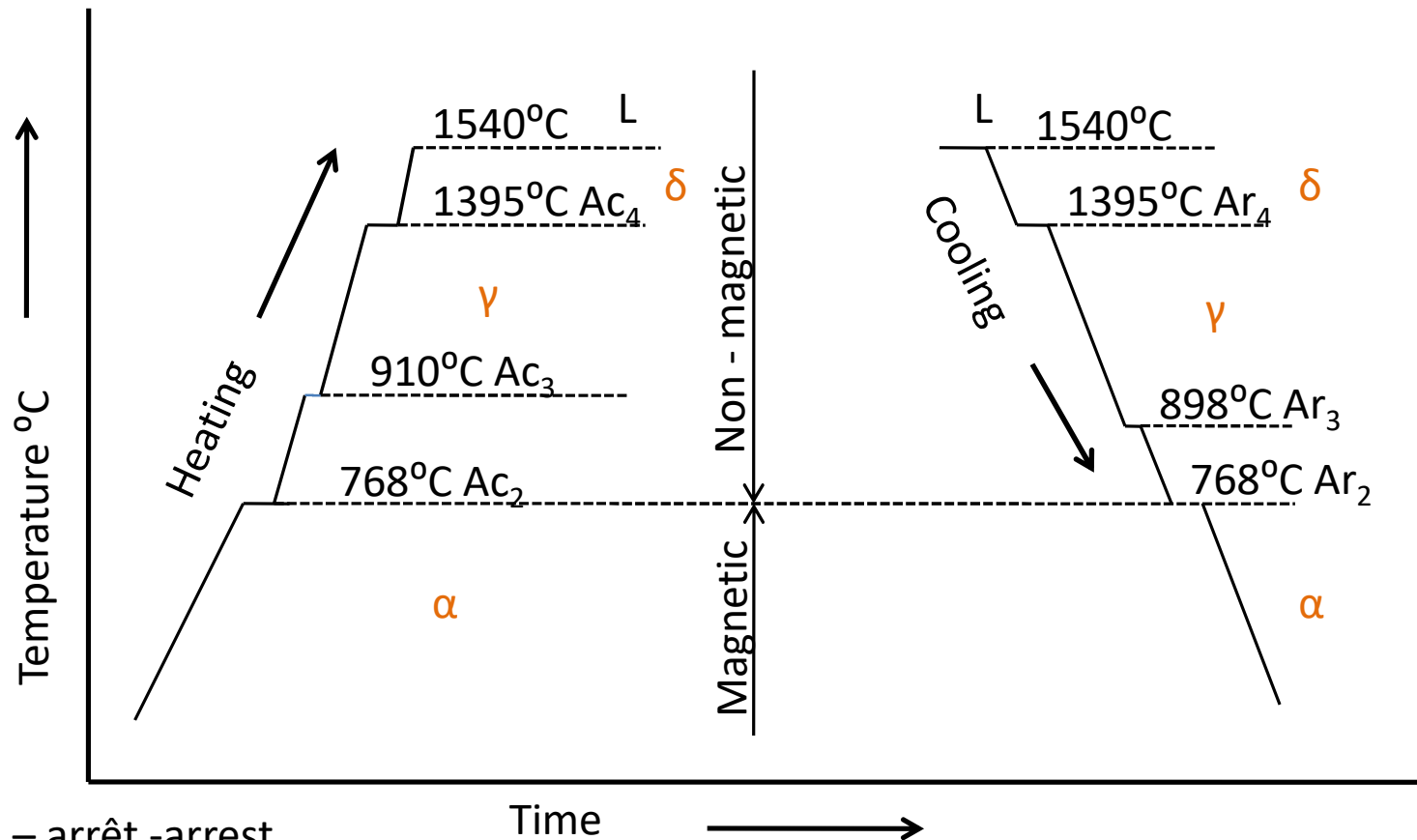
**Plutonium**

6 allotropy (RT to  $T_m$  --640°C)

Name	Crystal structure	Temp. range	No. of atoms in unit cell	Atomic packing density
$\alpha$ -Fe	BCC	< 910 °C	2	0.68
$\gamma$ -Fe	FCC	910 – 1394 °C	4	0.74
$\delta$ -Fe	BCC	1394 – 1539 °C	2	0.68

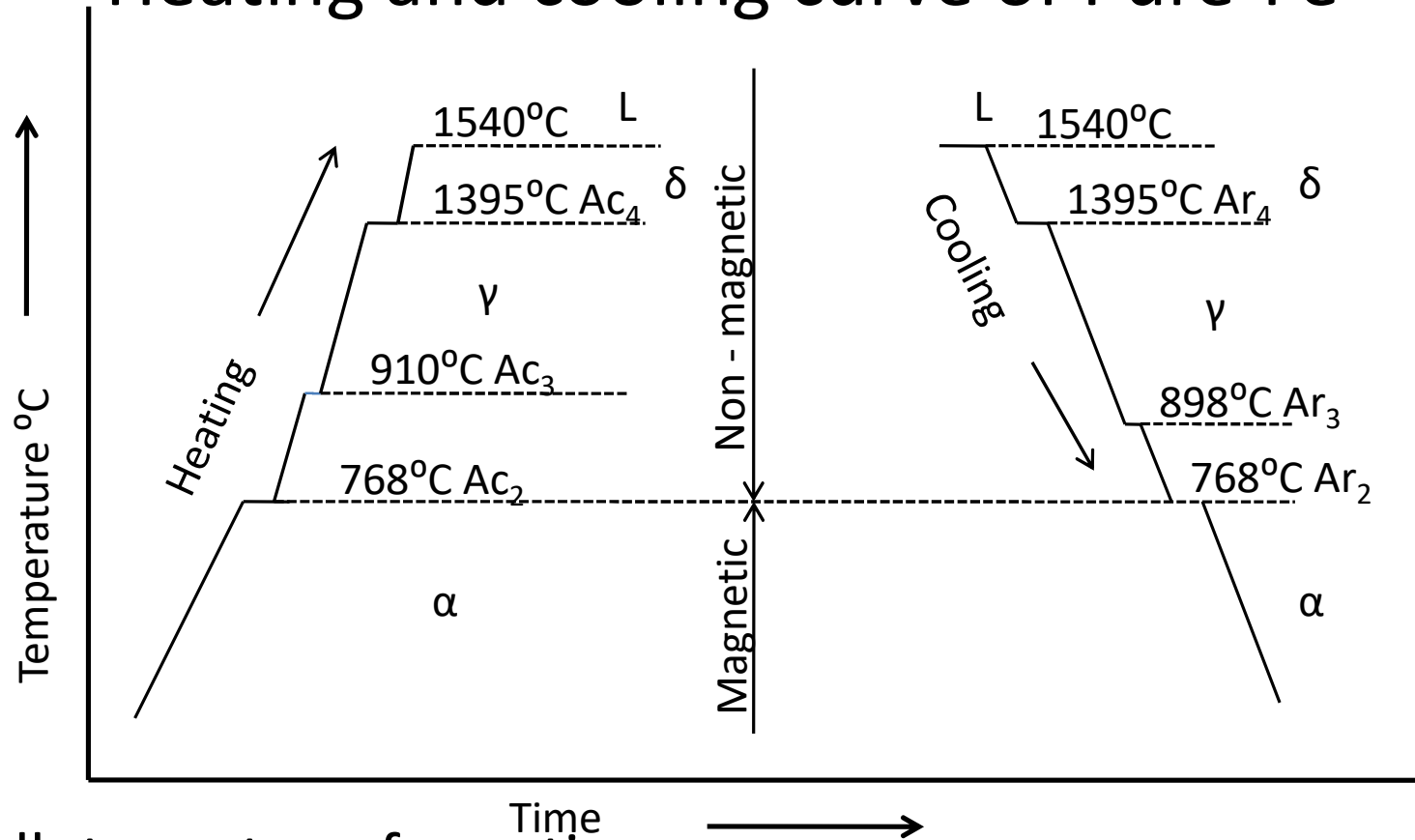
Allotropy transition can be abrupt or sluggish  
Volume change take place during transition

# Heating and cooling curve of Pure-Fe



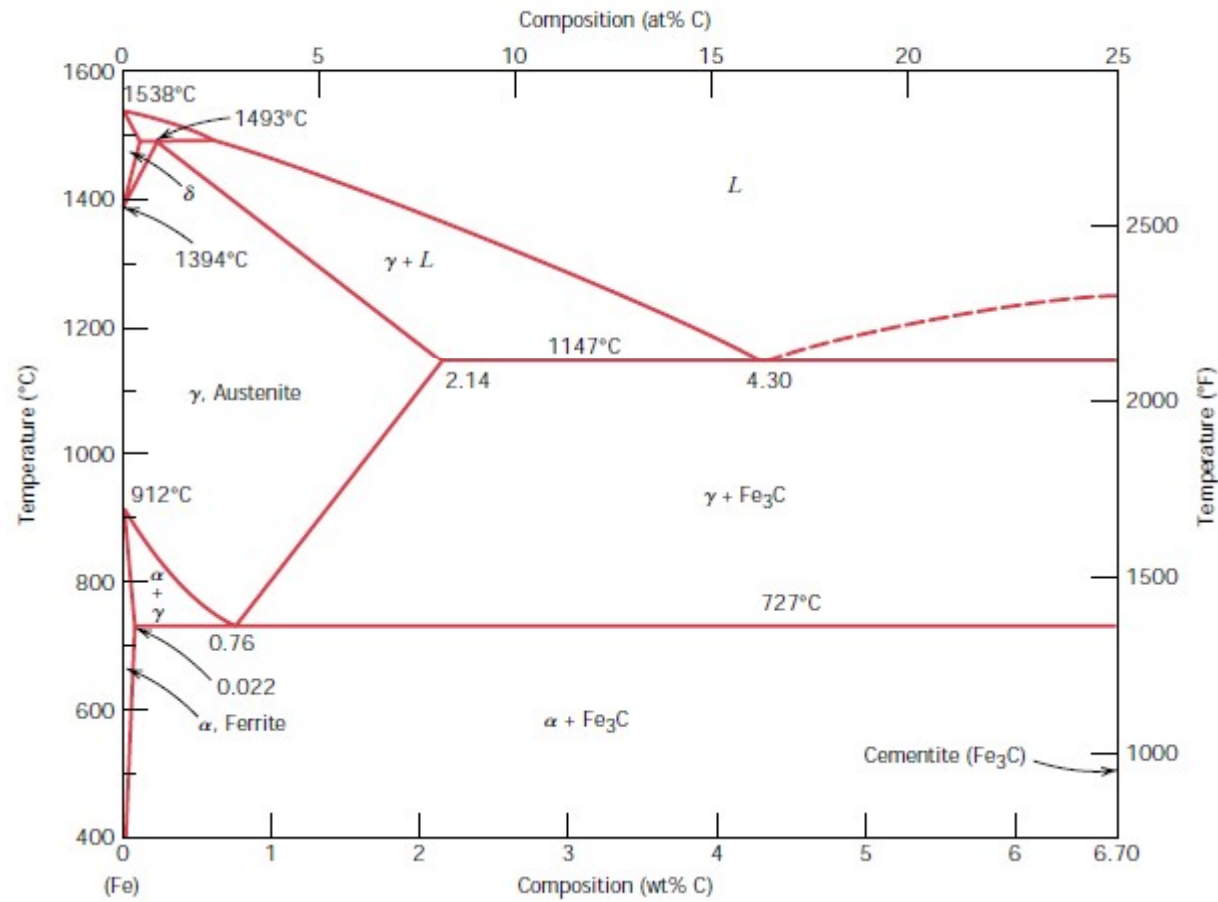
A – arrêt -arrest  
 r – refroidissement –cooling  
 c – chauffage - heating  
 French word in cooling

## Heating and cooling curve of Pure-Fe



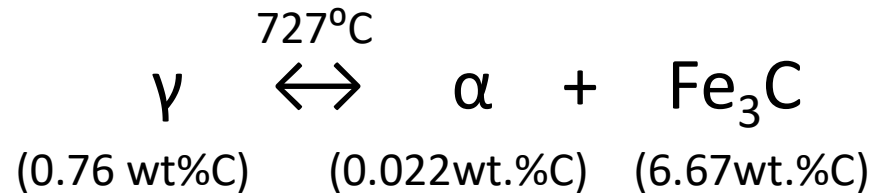
- Allotropy transformation occurs
  - Below equilibrium temperature during cooling
  - Above equilibrium temperature during heating
 These temperature lags called as **thermal hysteresis**

# Fe-Fe<sub>3</sub>C Diagram

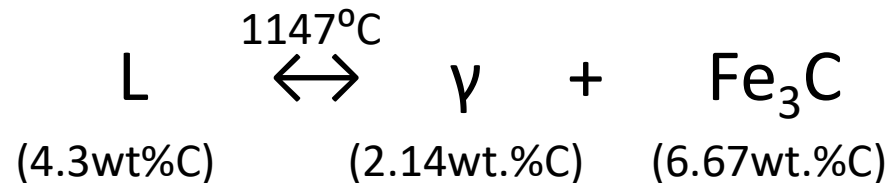


# Invariant Reactions

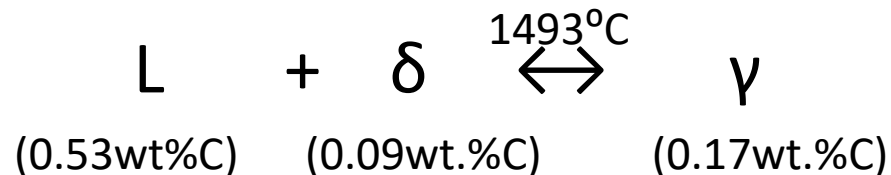
- Eutectoid Reaction



- Eutectic Reaction



- Peritectic Reaction





# Critical Temperatures in Fe-Fe<sub>3</sub>C diagram

## Notation

$A_0$  - Curie temperature of cementite

Magnetic cementite  $\xrightarrow{210^\circ\text{C}}$  Non-magnetic cementite

$A_1$  - eutectoid transition temperature

$\gamma\text{-Fe} \xrightarrow{727^\circ} \alpha\text{-Fe} + \text{Fe}_3\text{C}$

$A_2$  - Curie temperature of Fe

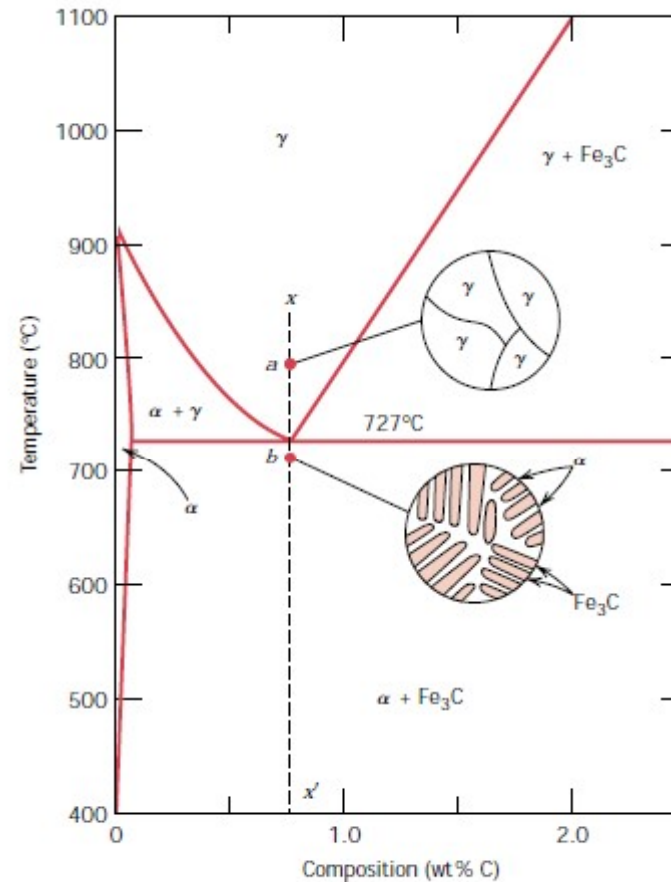
Ferromagnetic ferrite  $\xrightarrow{768^\circ\text{C}}$  Paramagnetic ferrite

$A_3$  - the temp. at which ferrite just starts forming from austenite on cooling a hypoeutectoid steel

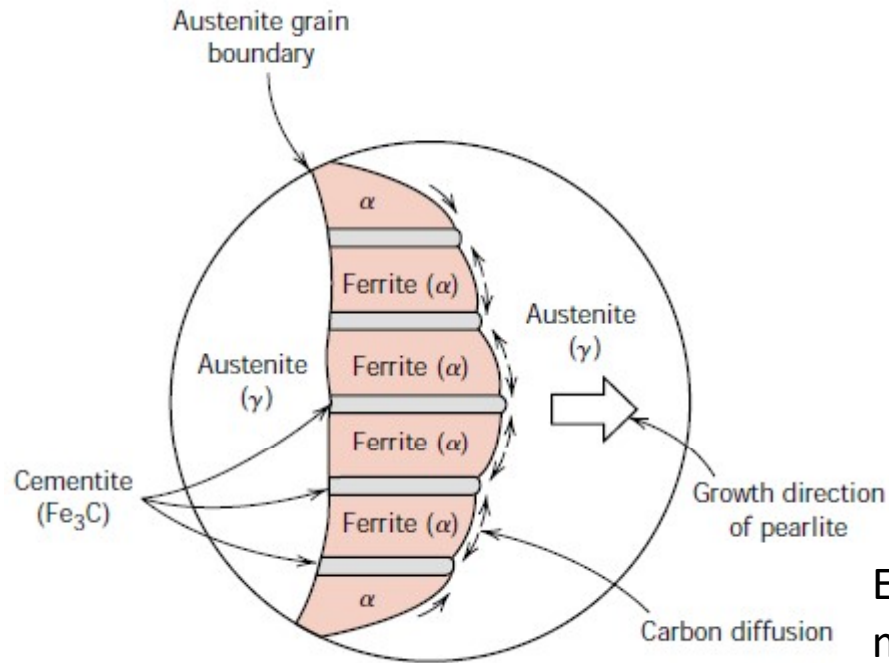
$A_4$  - the temp. at which  $\delta$ -Ferrite starts forming from austenite on heating

$A_{c_m}$  - the temp. at which cementite starts to forming from austenite on cooling a hypereutecoid steel

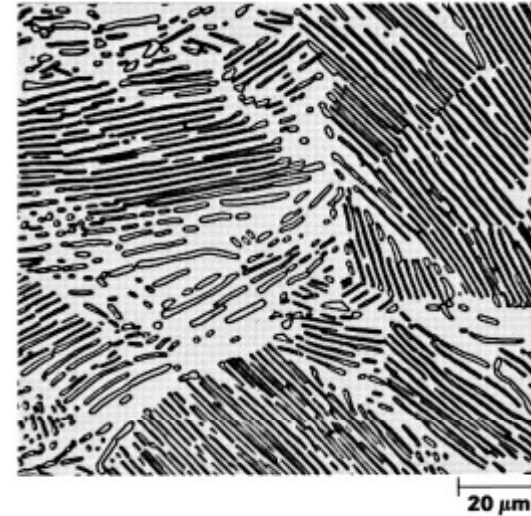
# Eutectoid Transformation



Schematic representations of the microstructures for an iron–carbon alloy of eutectoid composition (0.76 wt% C) above and below the eutectoid temperature.



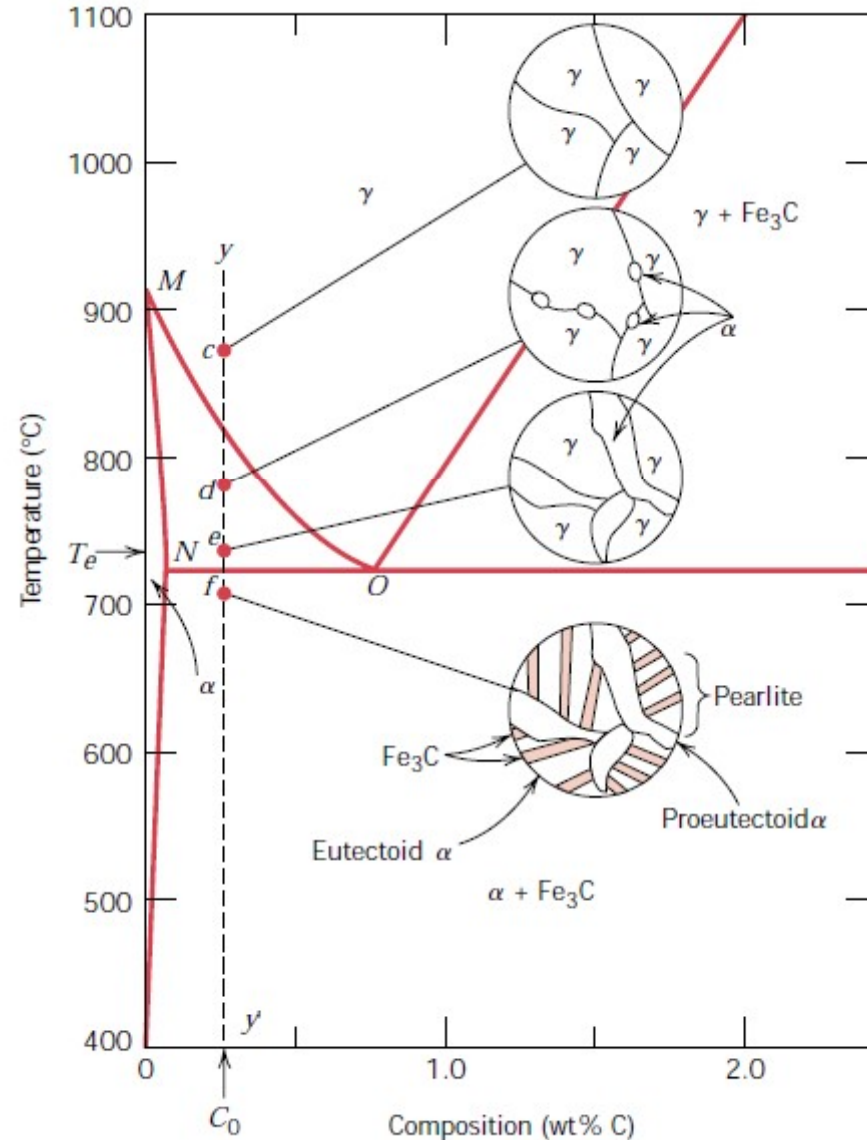
Schematic representation of the formation of pearlite from austenite; direction of carbon diffusion indicated by arrows.

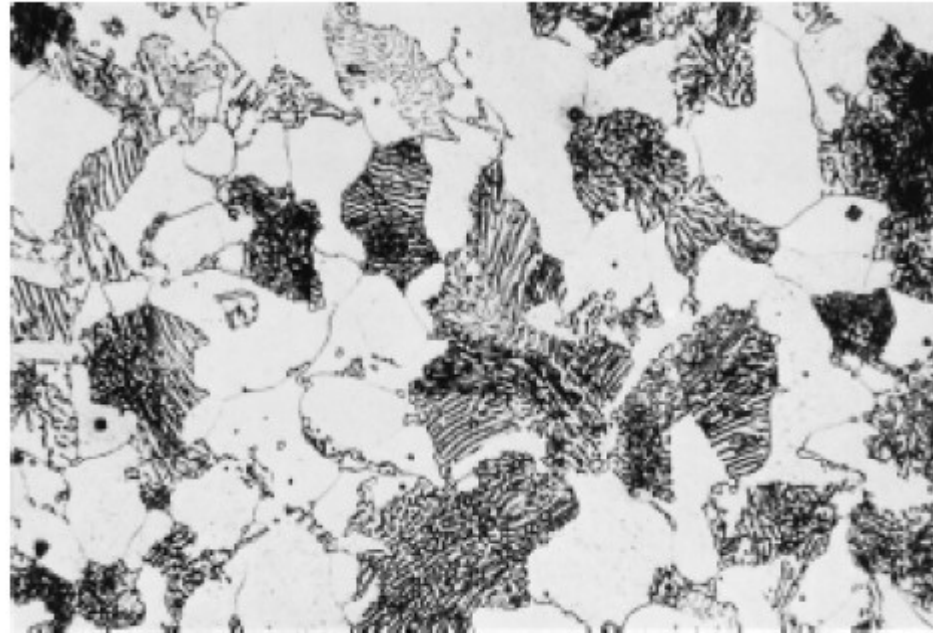


Eutectoid steel showing the pearlite microstructure consisting of alternating layers of ferrite (the light phase) and  $\text{Fe}_3\text{C}$  (thin layers most of which appear dark).

# Hypo-eutectoid Transformation

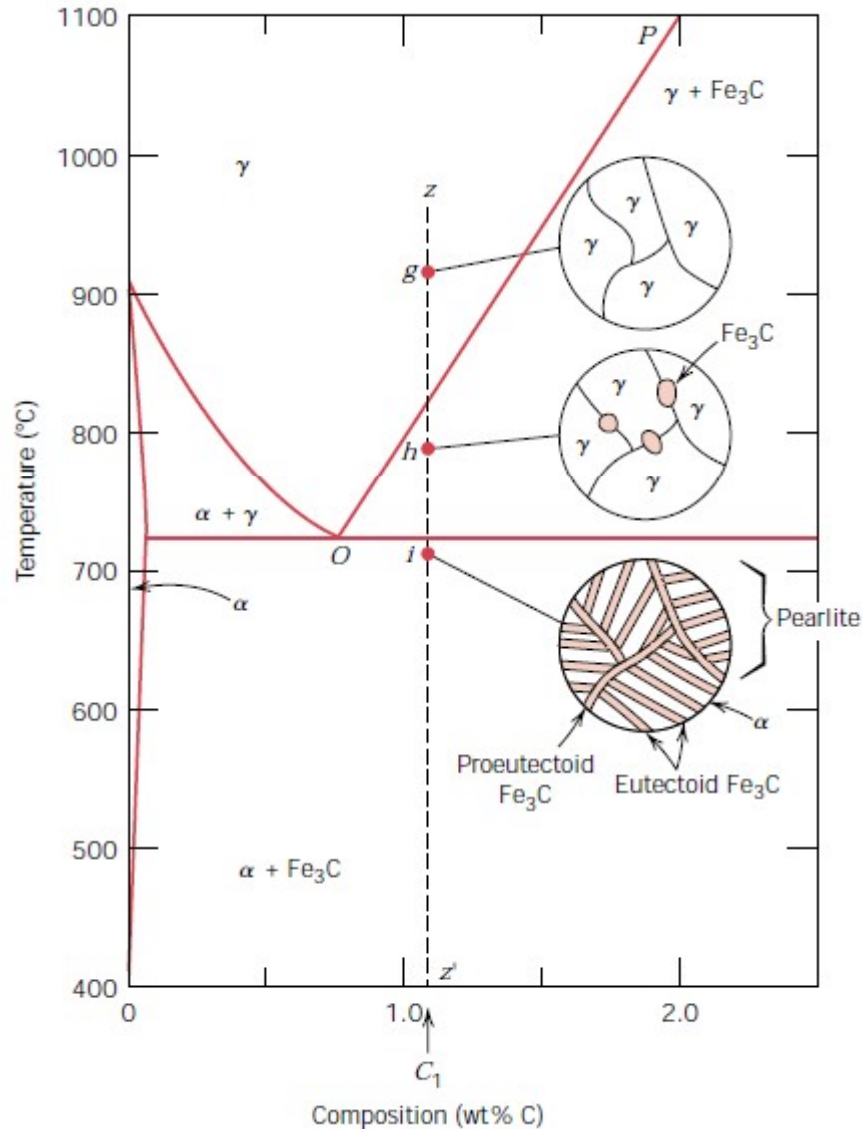
Schematic representations of the microstructures for an iron–carbon alloy of hypoeutectoid composition  $C_0$  (containing less than 0.76 wt% C) as it is cooled from within the austenite phase region to below the eutectoid temperature.





0.38 wt% C steel having a microstructure consisting of pearlite and proeutectoid ferrite.

# Hyper-eutectoid Transformation



Schematic representations of the microstructures for an iron-carbon alloy of hypereutectoid composition  $C_1$  (containing between 0.76 and 2.14 wt% C), as it is cooled from within the austenite phase region to below the eutectoid temperature.



I  
V  
C  
F  
I  
S

1.4 wt% C steel having a microstructure consisting of a white proeutectoid cementite network surrounding the pearlite colonies.

# Effect of Alloying Elements in Steel

Alloying elements affects

- Relative stabilities of ferrite and austenite
- Critical temperatures ( $A_1$ ,  $A_3$ ,  $A_4$  and  $A_{c_m}$ )
- Carbon content

Types:

- Ferrite stabilizers
- Austenite stabilizers



# Ferrite stabilizers

Elements which stabilizing ferrite phase are called **ferrite stabilizers**

- Ex.: Cr, W, Mo, V & Si

Ferrite stabilizers are,

- More soluble in  $\alpha$ -Fe than  $\gamma$ -Fe
- Mostly in BCC crystal structure
- Decreases the amount of C in  $\gamma$ -Fe
- Reduces the austenite region in Fe-Fe<sub>3</sub>C phase diagram by lowering  $A_4$  & raising  $A_3$ .

Quantities of elements required for stabilization of ferrite:

Element	Cr	Si	W	Ti	Mo	V
Comp. (wt.%)	12.8	2.0	6	0.75	4	2

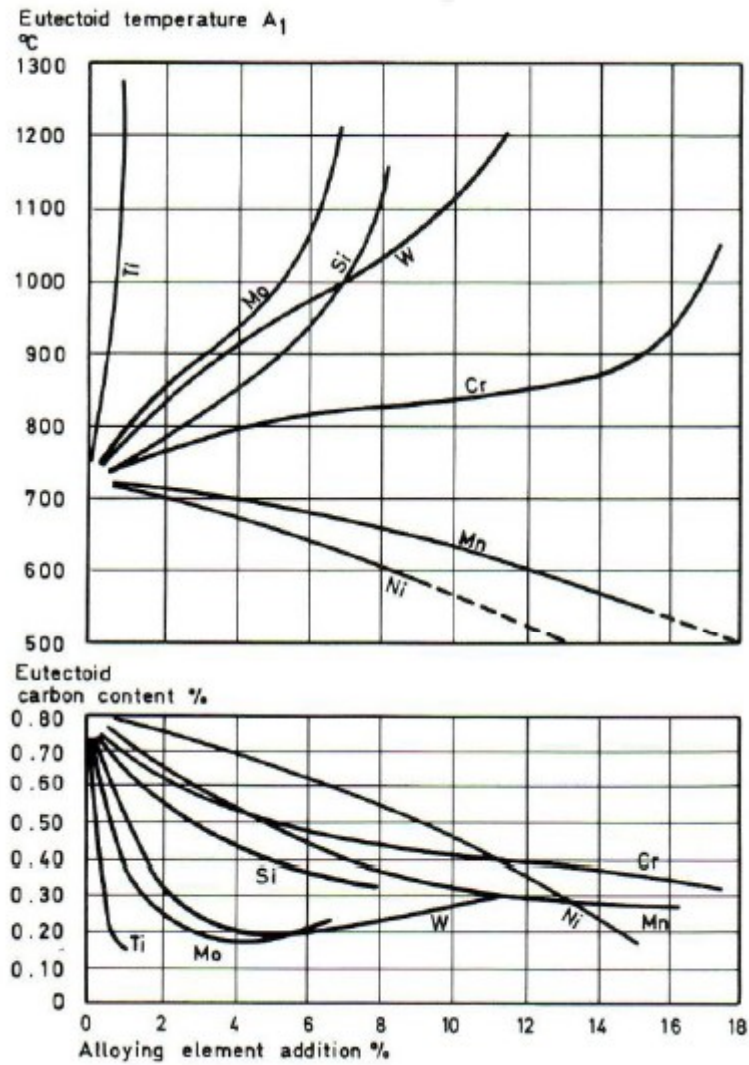
# Austenite stabilizers

Elements which stabilizing austenite phase are called **austenite stabilizers**

Ex.: Ni, Mn

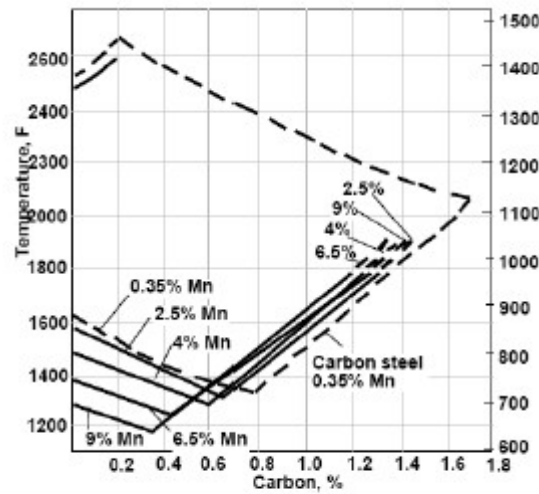
Austenite stabilizers are,

- More soluble in  $\gamma$ -Fe than  $\alpha$ -Fe
- Mostly in FCC crystal structure
- Decreases the amount of C in  $\alpha$ -Fe
- Enlarge the austenite region by shifting  $A_4$  upward and  $A_3$  &  $A_1$  downwards. – even make austenite stable in room temp.

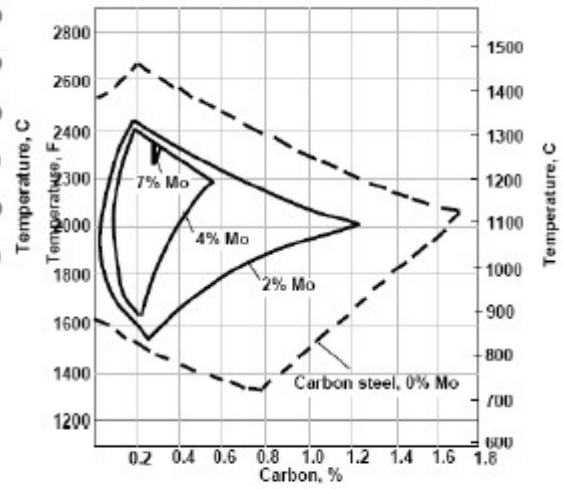


Influence of alloying element in eutecoid Transformation temperature

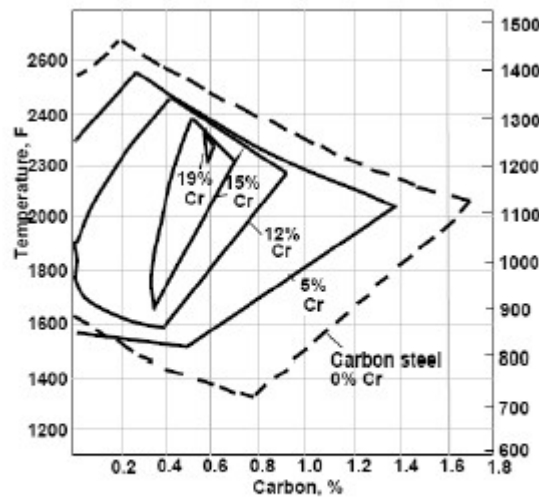
Influence of alloying element in gamma phase field.



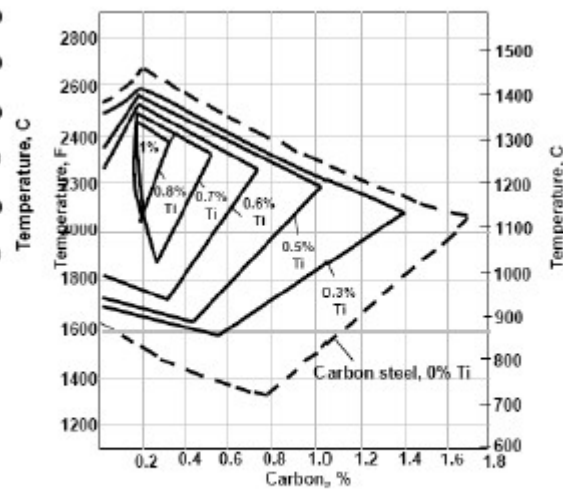
(a)



(b)



(c)



(d)

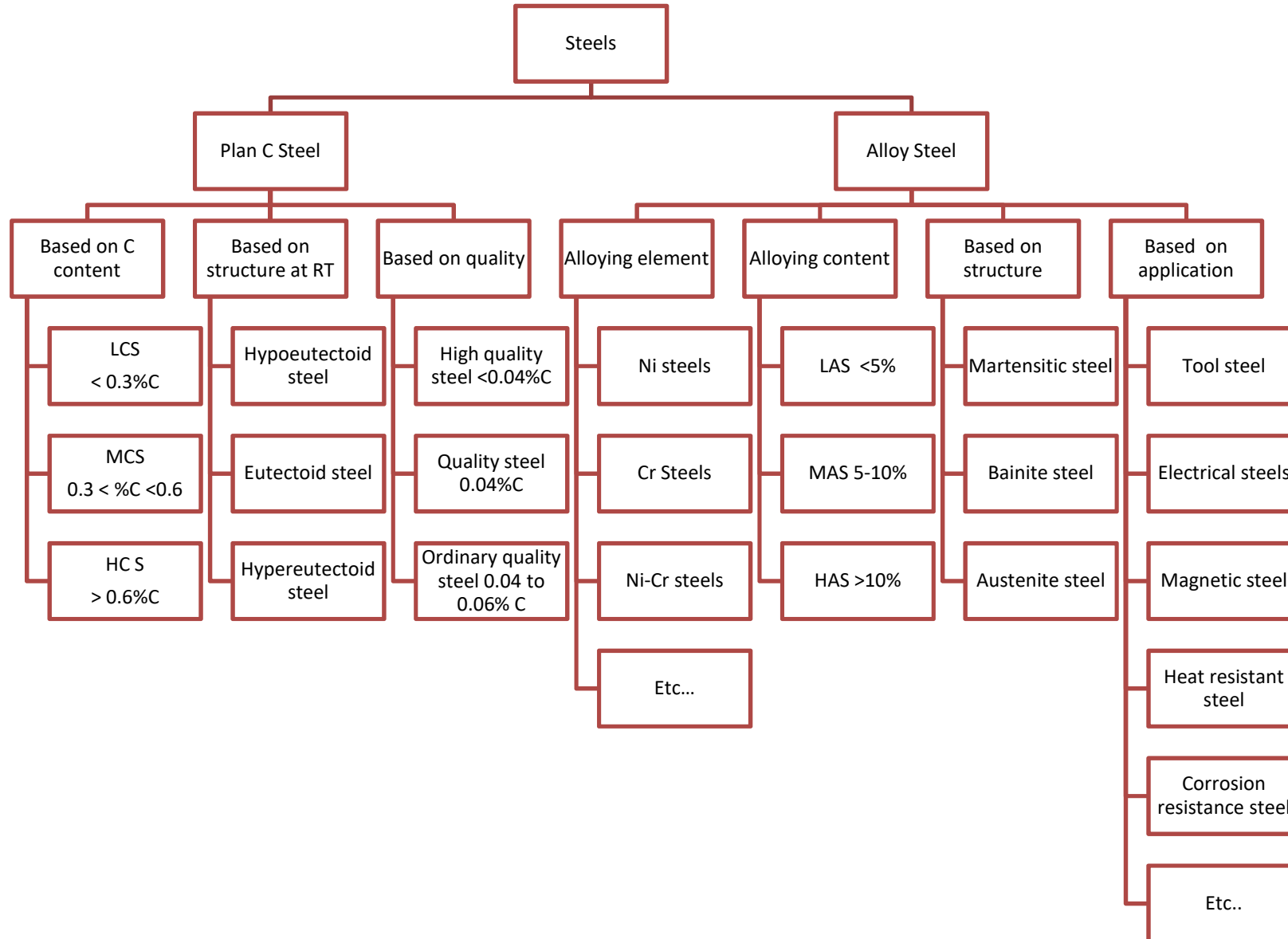
**Carbon Equivalent** (CE) is an empirical value in weight percent, relating the combined effects of different alloying elements used in the making of **carbon** steels to an **equivalent** amount of **carbon**. This value can be calculated using a mathematical equation.

Example: AWS states that for an equivalent carbon content above 0.40% there is a potential for cracking in the [heat-affected zone](#) (HAZ) on [flame cut](#) edges and welds.

$$CE = \%C + \left( \frac{\%Mn + \%Si}{6} \right) + \left( \frac{\%Cr + \%Mo + \%V}{5} \right) + \left( \frac{\%Cu + \%Ni}{15} \right)$$

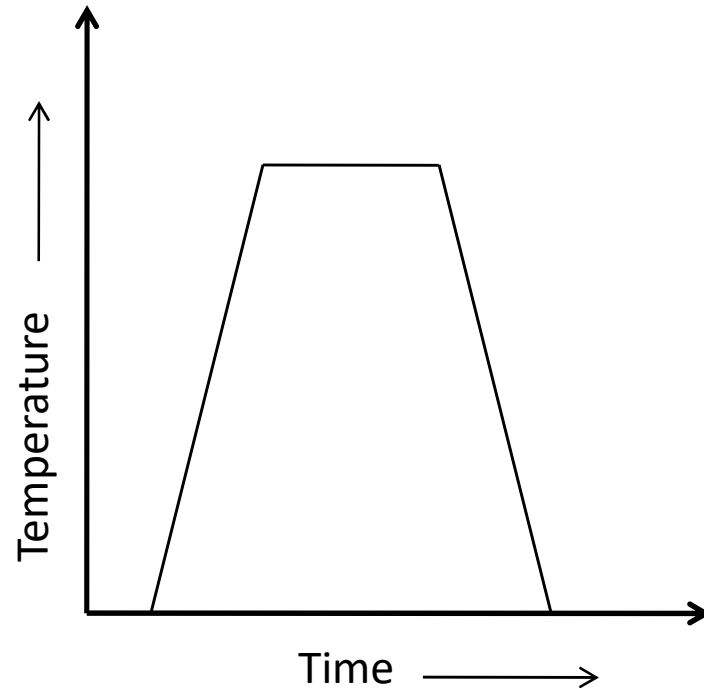
In high strength steels, CE = 0.5 which lead to cracking.

# Classification of Steel



# Heat Treatment

The heat treatment includes heating and cooling operations or the sequence of two or more such operations applied to any material in order to modify its metallurgical structure and alter its physical, mechanical and chemical properties.

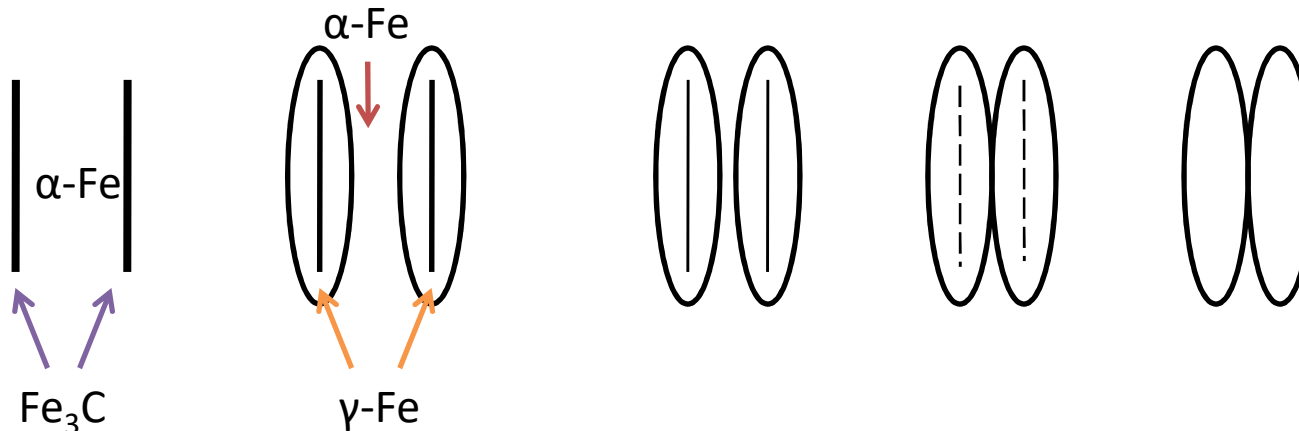




# Formation of Austenite on Heating

## Eutectoid steel:

1. Upto 200°C, C diffusion rate is insignificant
2. At 727°C,  $\alpha$ -Fe changes into  $\gamma$ -Fe.
3. The growth rate of austenite is higher than dissolution cementite into austenite.
4. Austenite formed at eutectoid temperature is not homogeneous



Hypo eutectoid and Hyper eutectoid steels:

1. These steels transformation into austenite different from eutectoid steel
2. In Hypoeutectoid steels,  $\text{Fe}_3\text{C}$  dissolves in to the ferrite which in turn transforms into austenite. Austenite nuclei form at ferrite grain boundary and then its grows.
3. In Hyper eutectoid steels, austenite grow by dissolving proeutectoid cementite

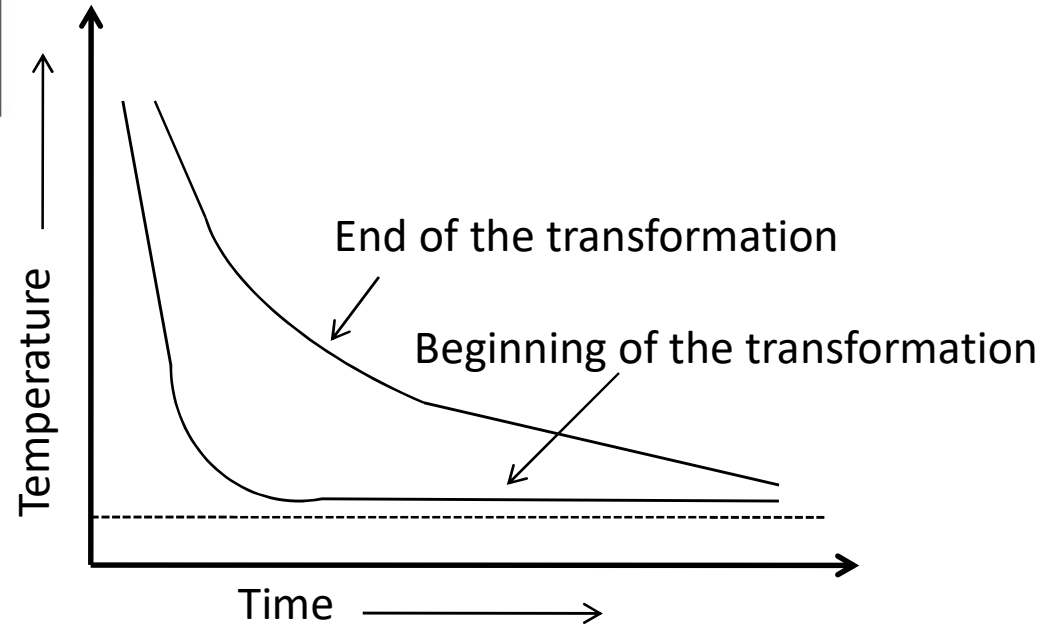
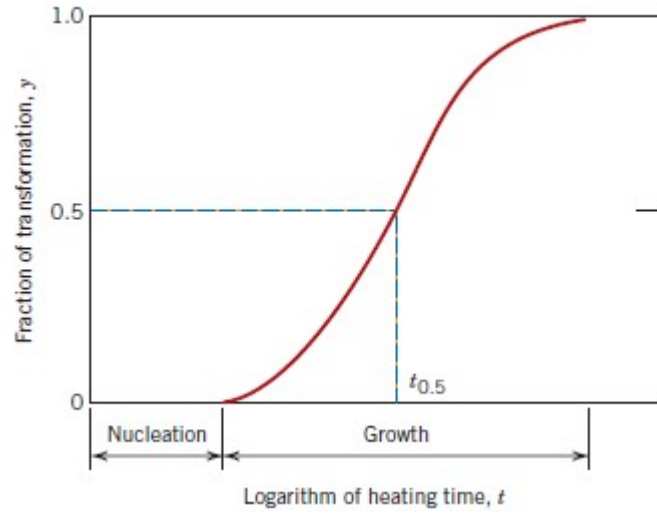
# Kinetics of formation of austenite

Heating eutectoid steel,

- Austenite formation take place by nucleation and growth
- Rate of nucleation or rate of growth or both → decides the kinetics of austenite formation

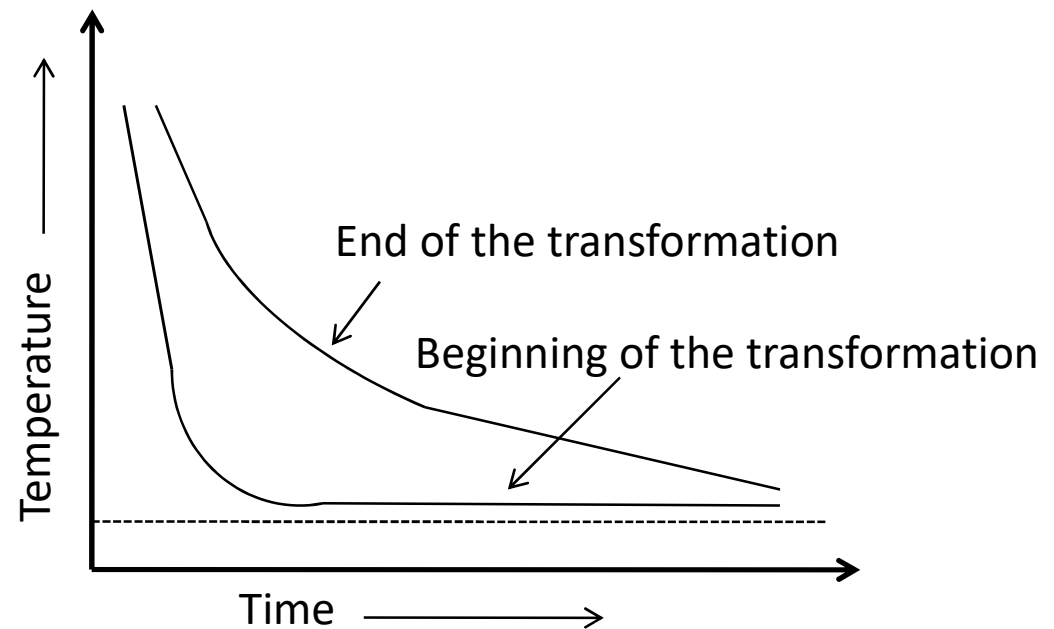
Factors

- The transformation temperature
- Holding time at transformation temperature
- Interface of ferrite and cementite



Effect of temperature on the time required for start and completion of transformation of pearlite to austenite

- Transformation completed short period in high temperature.
- For higher heating rates, nucleation starts at high temperature and vice versa.
- For all the heating rates, austenite formation taking place over a time period.



Effect of temperature on the time required for start and completion of transformation of pearlite to austenite

# Isothermal Transformation



Fig. 1 : Salt bath I -austenitisation heat treatment.  $T = 780^{\circ}\text{C}$



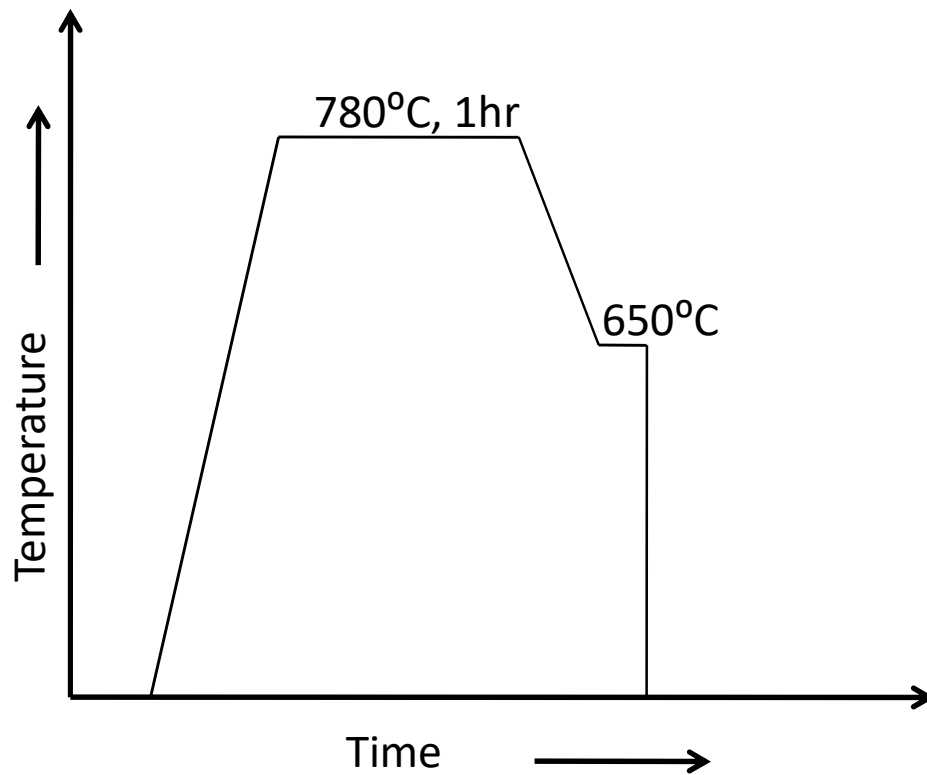
Fig. 2 : Bath II low-temperature salt-bath for isothermal treatment.  $T = 650^{\circ}\text{C}$

# Isothermal Transformation

For eutectoid steel,

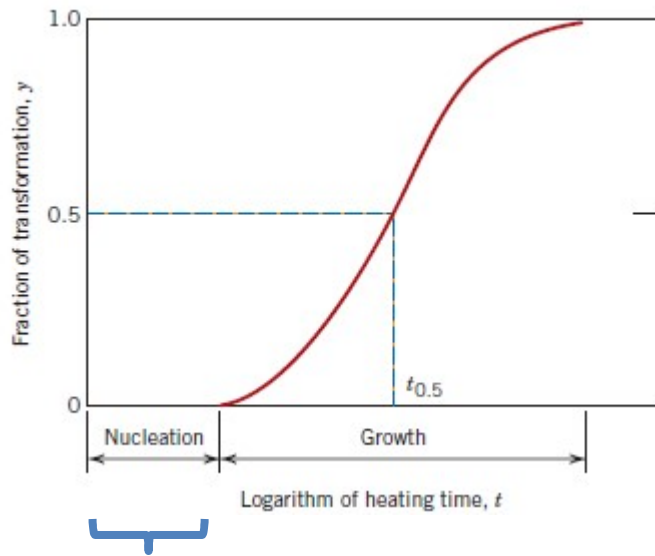
- In bath I,  $T=780^{\circ}\text{C}$  for  $\sim 1\text{hr}$ .
- Sample moved from bath I to bath II
- In bath II, at  $T=650^{\circ}\text{C}$ .
- After specified time, the sample are removed and quenched in water.
- Study the microstructure of the sample using metallographic techniques

Repeat the experiment with varying time period in bath II



- Why 780°C ?
- Why 1hr?
- Why 650°C?
- What will happen if bath II temp. is 25°C?





t - Incubation period

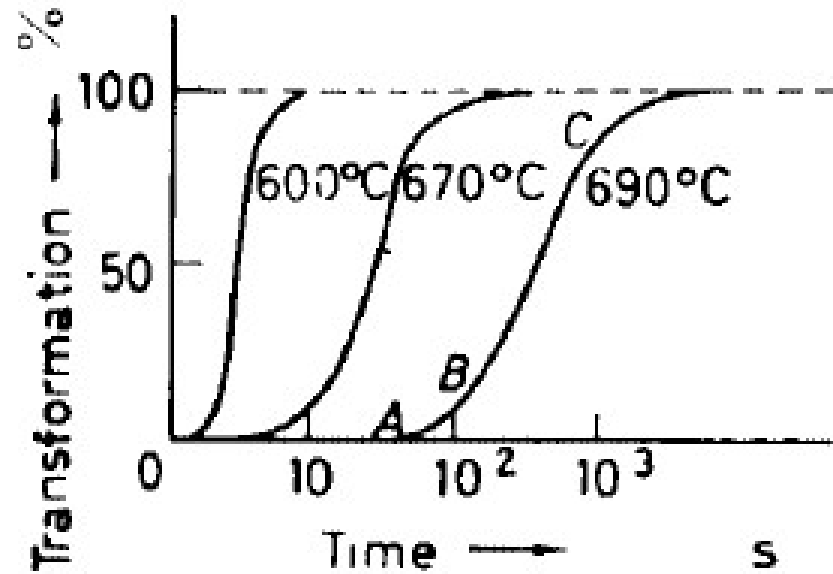
Isothermal Transformation curve

Or

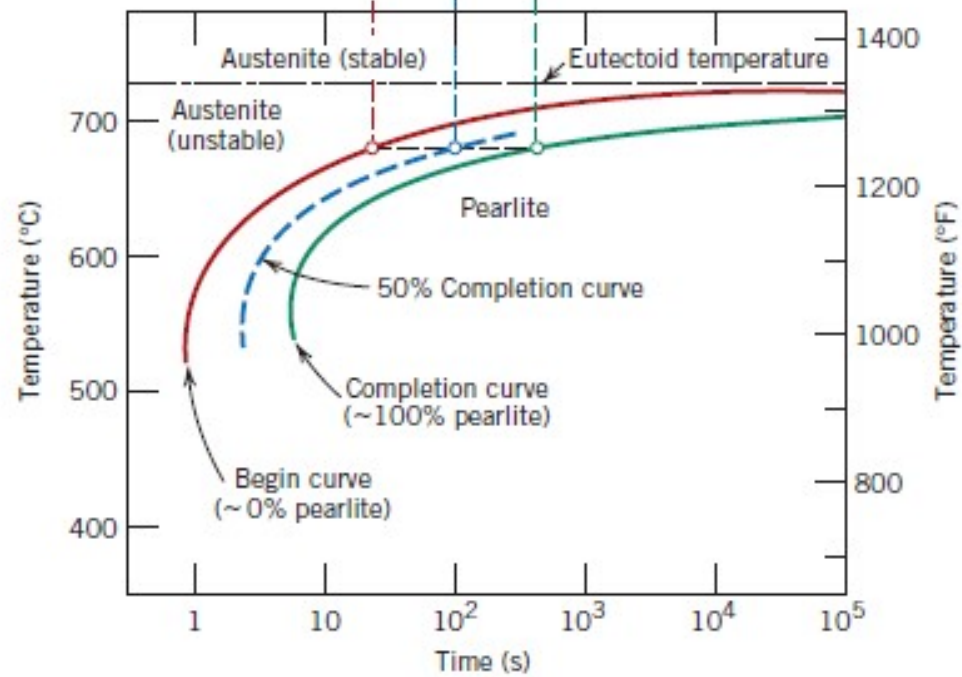
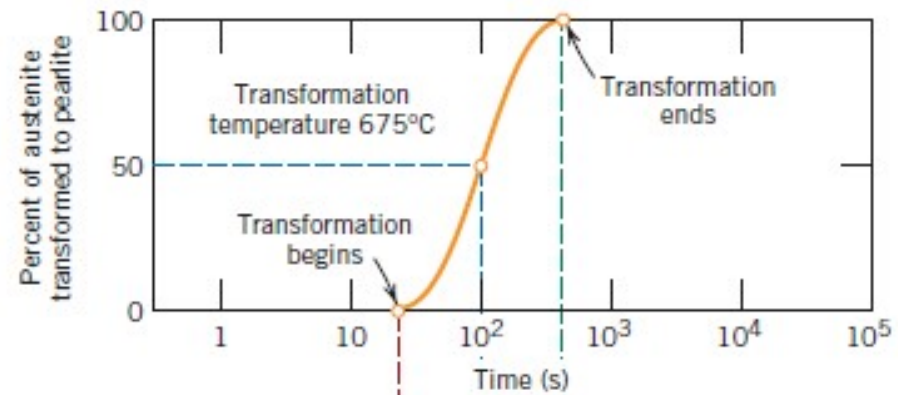
C - Curve

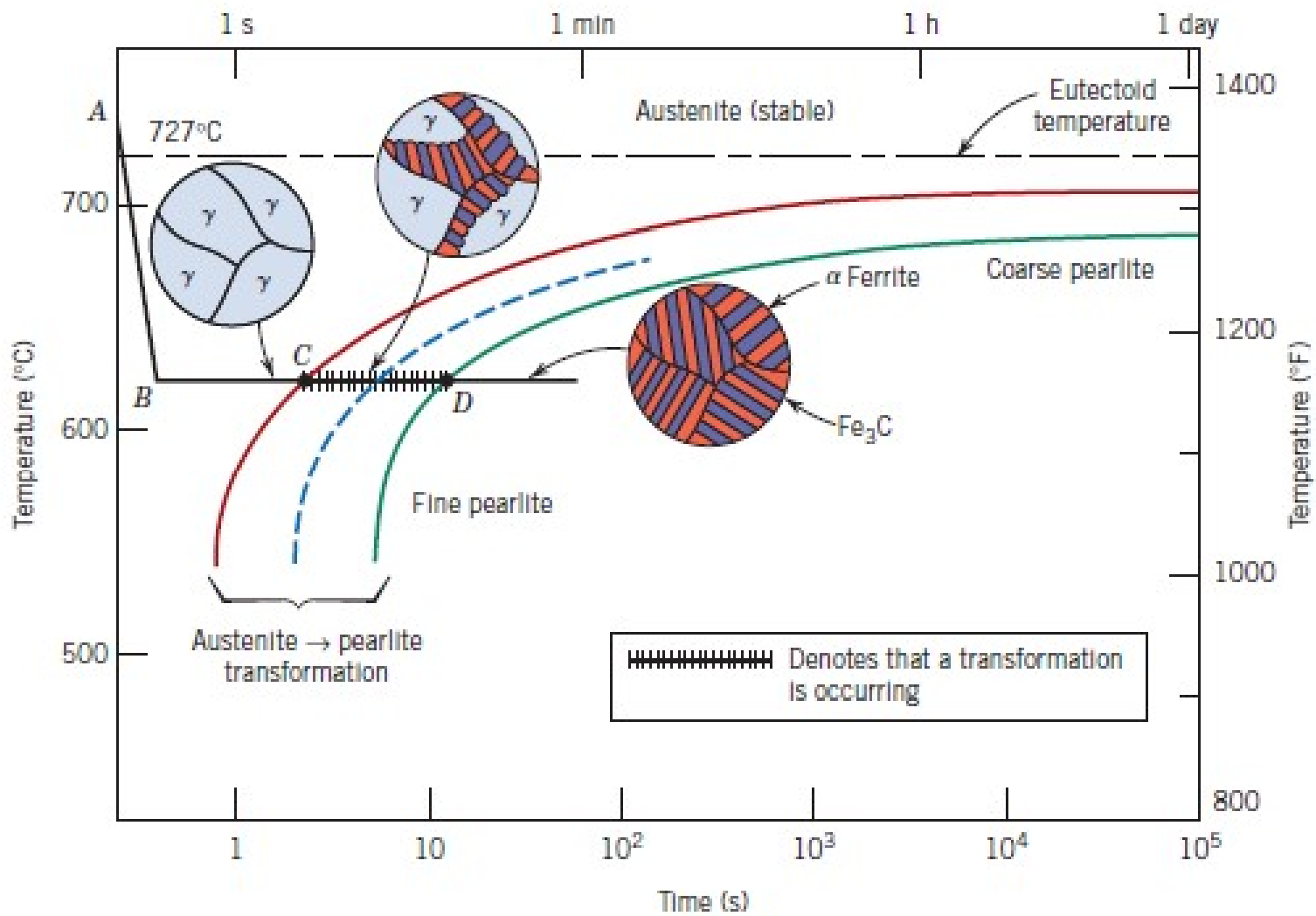
Or

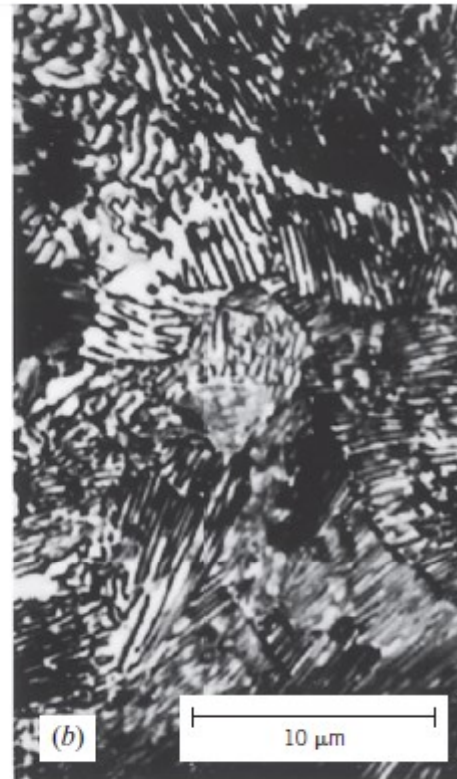
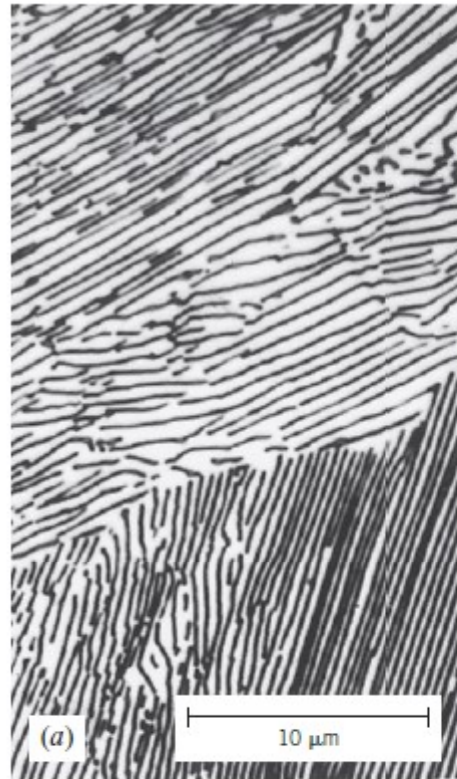
S - Curve



*amount of pearlite formed with time*

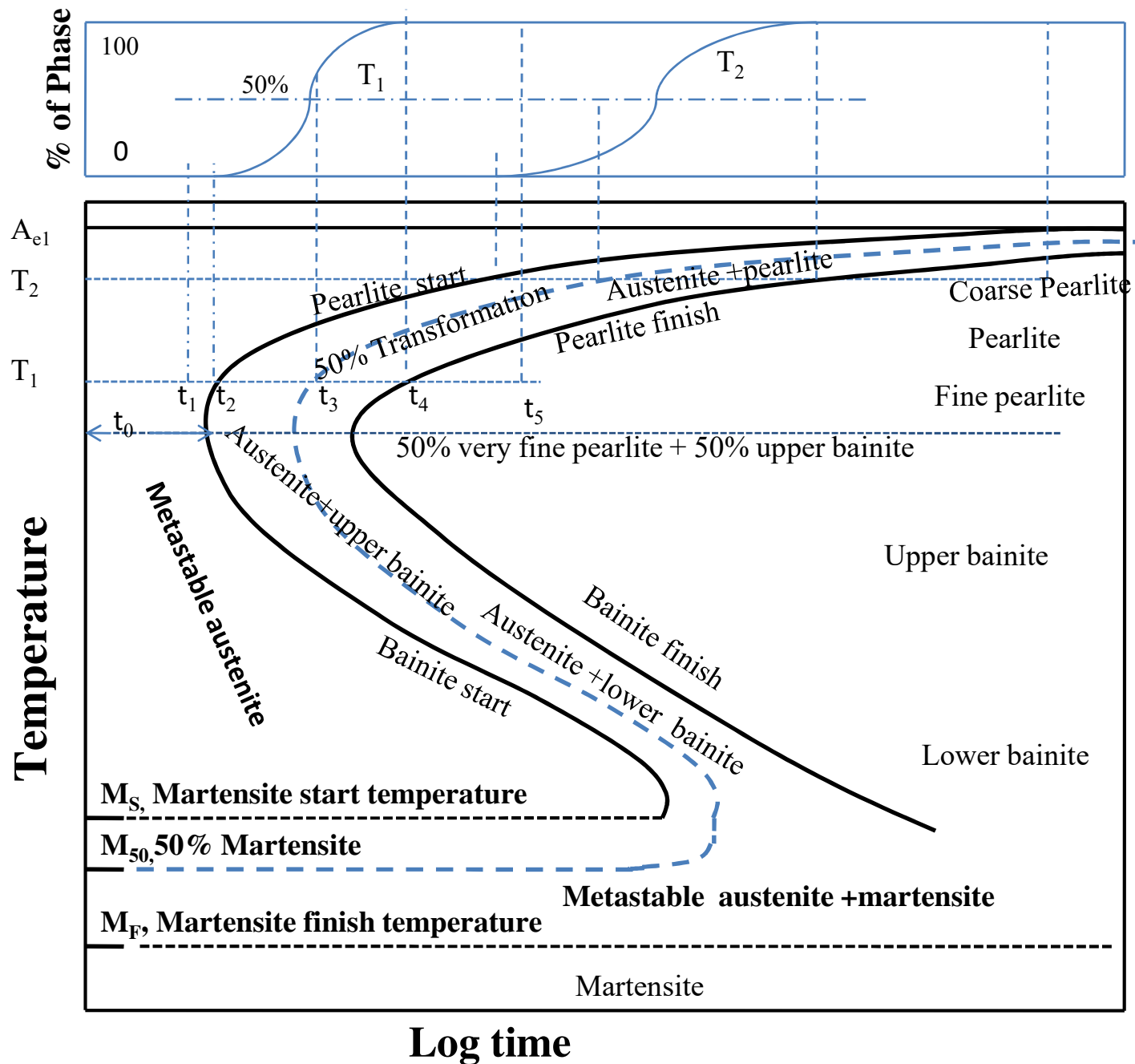






Coarse pearlite    Fine pearlite

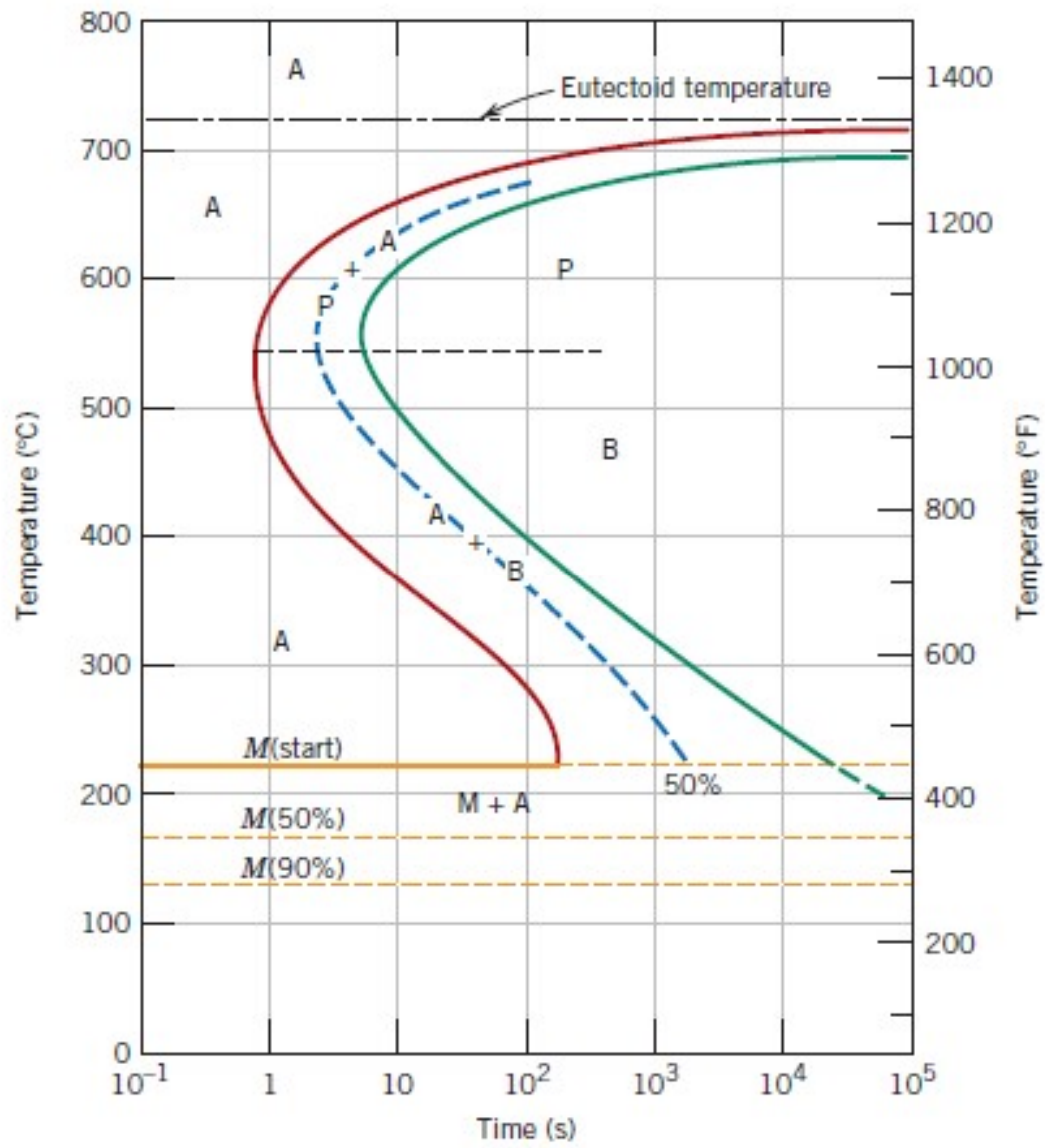
**Figure: TTT Diagram for plain carbon eutectoid steel**



At  $t_1$ , incubation period for pearlite,  
 $t_2$ , pearlite starting time  
 Pearlite finish time =  $t_4$   
 Minimum incubation period  $t_0$  at the nose of the TTT diagram,

**Hardness** ↓

$M_s$  = Martensite start temperature  
 $M_{50}$  = temperature for 50% martensite formation  
 $M_f$  = martensite finish temperature





# Factors Affecting TTT Diagram

- Composition of steel
  - Amount of carbon and alloying elements
    - C or alloying element ↑ es 'S' progressively lowered
    - $M_s$  temperature decreases
  - Austenite stabilizers (Ni, Mn etc.) lower  $Ac_3$  and  $Ac_1$  temperatures too
  - Ferrite stabilisers (V, Mo, W, Cr etc) raise  $Ac_3$  and  $Ac_1$  temperatures and such steels show two 'C' curves (one for pearlite and other for bainite transformations)



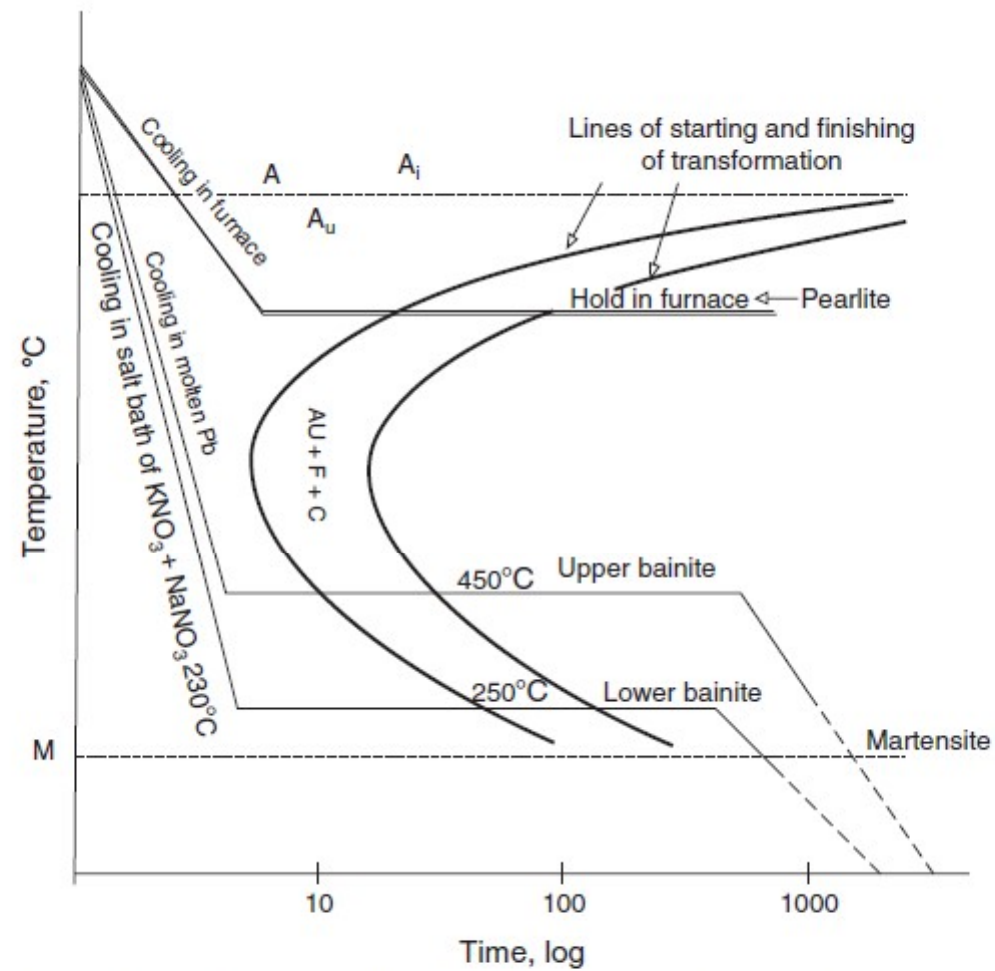
- Carbon

<b>Hypo eutectoid steel</b>	<b>Hyper eutectoid steel</b>
Ferrite is the nucleating phase	Cementite is the nucleating phase
Nose of 'S' curve shift to left hand side	Nose of 'S' curve shift to left hand side

- For bainite formation, ferrite is nucleating phase
- If amount of C increases, the bainitic part of 'S' curve shifts towards the right. i.e. bainitic transformation is uniformly retarded.

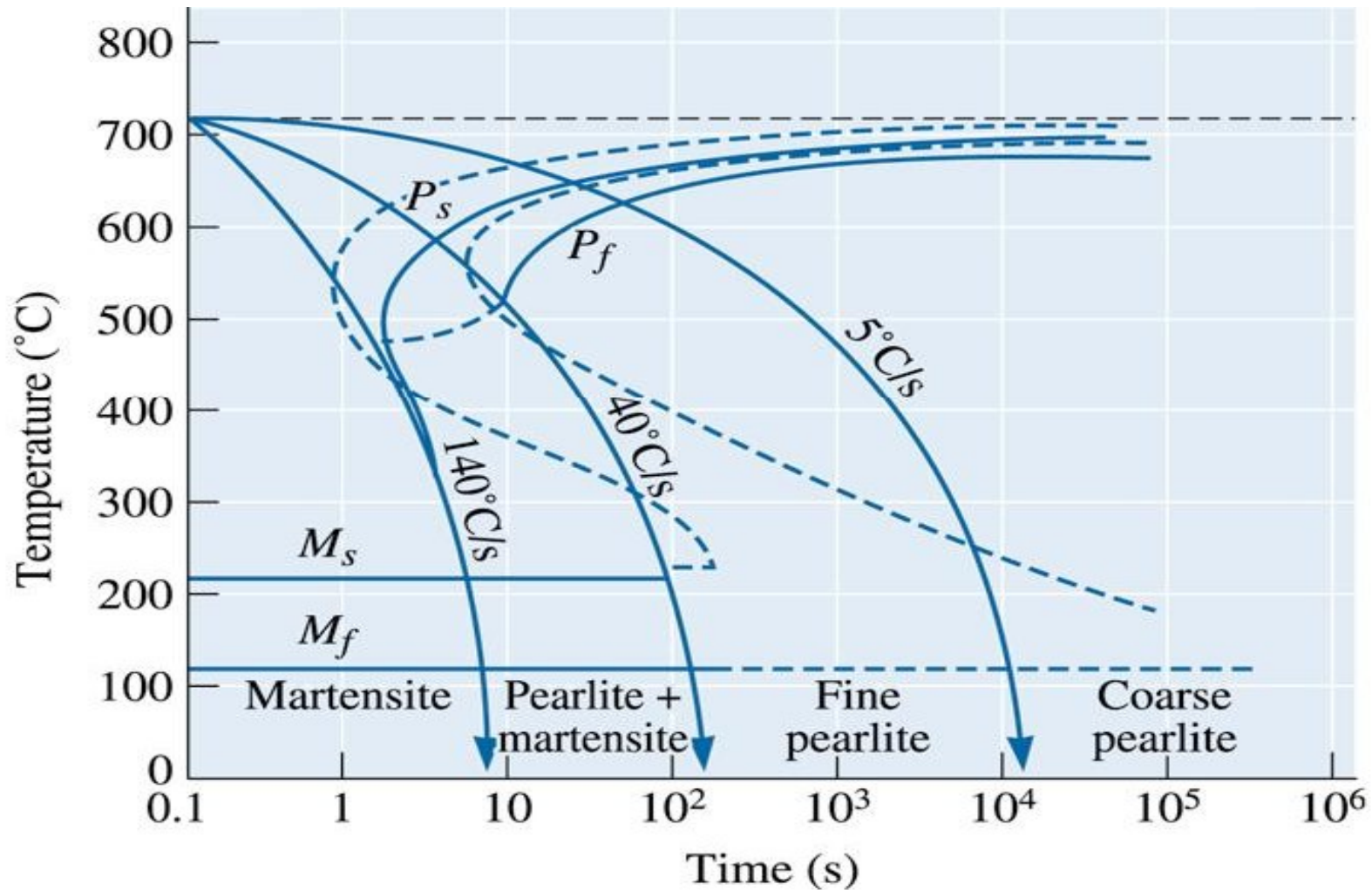
# TTT Diagram for Alloy Steel

- Alloying Elements
  - Except Co all other alloying elements shift 'S' curve to the right
  - Carbide forming element which dissolved in austenite stabilize austenite phase which shift 'S' curve to the right.
    - The austenite phase tries to decompose to ferrite and alloyed carbide
    - Substitutional element diffusion is slow
    - Diffusion of C too slow, due to carbide forming elements
    - Reduce the allotropic change by solute drag effect on its interface boundary.



**FIGURE 3.13** Isothermal transformation diagram for a eutectoid composition steel. A, stable austenite; A<sub>u</sub>, undercooled austenite; F, ferrite; C, carbide.

# Continuous Cooling Transformation Diagram



The CCT diagram (solid lines) for a 1080 steel compared with the TTT diagram (dashed lines).

