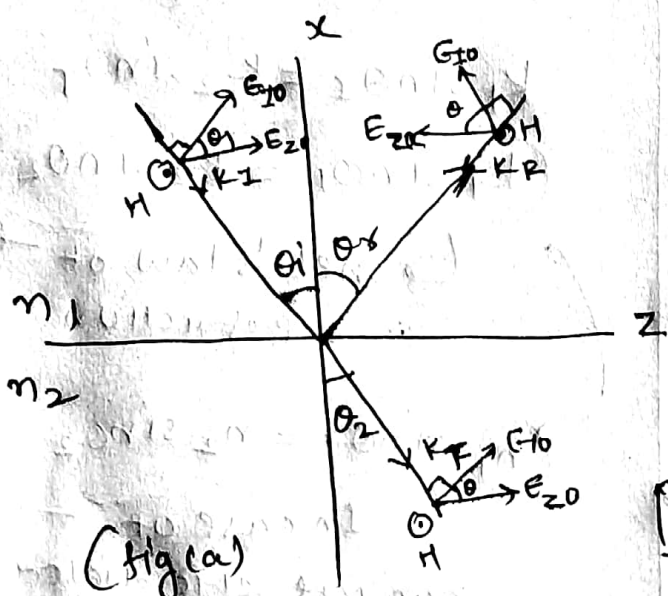


# Plane wave Reflection at oblique Incidence

(1) Relation between Incident ( $\theta_i$ ), Reflected ( $\theta_r$ ) and transmitted angle ( $\theta_t$ )

(2) To determine reflection & transmission Coefficient



(fig a)  
Parallel Polarization  
E in plane of incidence  
(Transverse magnetic)

**P-polarization**

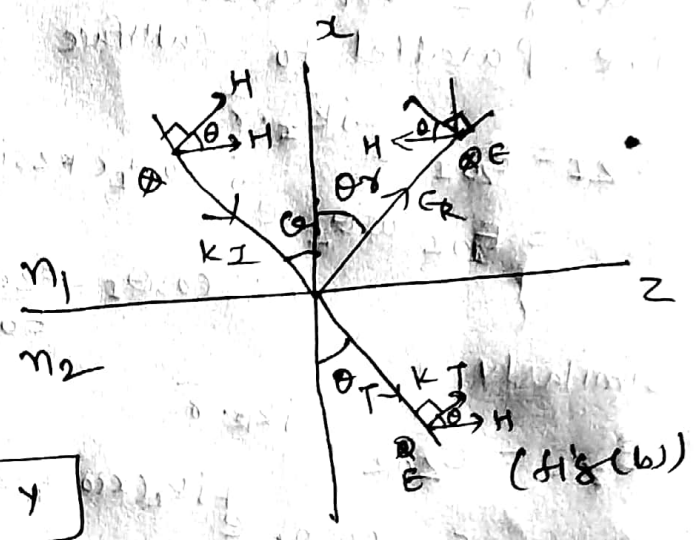
E || plane of incidence  
H  $\perp$  plane of incidence

$$E_I = E_{0I} e^{-j\vec{k}_I \cdot \vec{r}}$$

$$E_R = E_{0R} e^{-j\vec{k}_R \cdot \vec{r}}$$

$$E_T = E_{0T} e^{-j\vec{k}_T \cdot \vec{r}}$$

where  $\vec{k}$  is pointing vector



Perpendicular polarization  
E perpendicular to plane of incidence  
(Transverse Electric)

**S-polarization**

E  $\perp$  plane of incidence  
H || plane of incidence

$$\vec{k}_I = k_I \cos \theta_I \hat{i} + k_I \sin \theta_I \hat{z}$$

$$\vec{k}_R = -k_R \cos \theta_R \hat{i} + k_R \sin \theta_R \hat{z}$$

$$\vec{k}_T = k_T \cos \theta_T \hat{i} + k_T \sin \theta_T \hat{z}$$

$$\vec{r} = x \hat{i} + z \hat{k}$$

Boundary conditions  
Projecting E components  
along z-direction  
i.e. parallel to interface

$$\begin{aligned} E_{zI} &= E_{z0I} e^{-j\vec{k}_I \cdot \vec{r}} \\ &= E_{z0I} \cos \theta_I e^{-jk_I(\cos \theta_I x + z \sin \theta_I)} \end{aligned}$$

( $\because \cos \theta_I = \frac{E_{z0I}}{E_{0I}}$ )

Similarly,

$$\begin{aligned} E_{zR} &= E_{z0R} e^{-j\vec{k}_R \cdot \vec{r}} \\ &= E_{0R} \cos \theta_R e^{+jk_R(x \cos \theta_R - z \sin \theta_R)} \end{aligned}$$

$$\begin{aligned} E_{zT} &= E_{z0T} e^{-j\vec{k}_T \cdot \vec{r}} \\ &= E_{0T} \cos \theta_T e^{jk_T(x \cos \theta_T + z \sin \theta_T)} \end{aligned}$$

Boundary condition for Tangential Electric field

$$E_{zI} + E_{zR} = E_{zT} \quad (\text{at } x=0)$$

$$\begin{aligned} &E_{0I} \cos \theta_I e^{-jk_I z \sin \theta_I} \\ &+ E_{0R} \cos \theta_R e^{-jk_R z \sin \theta_R} \\ &= E_{0T} \cos \theta_T e^{-jk_T z \sin \theta_T} \end{aligned}$$

Independent  
of z

To make above Eqn. hold for all value of all phase terms Equate  
 $k_I z \sin \theta_I = k_R z \sin \theta_R$   
 $= k_T z \sin \theta_T$

But  $k_I = k_R = k_1$   
&  $k_T = k_2$

$$k_1 \sin \theta_I = k_2 \sin \theta_T$$

$$k_1 \sin \theta_I = k_2 \sin \theta_T$$

↳ Snell's law of refraction

$$n_1 \sin \theta_I = n_2 \sin \theta_T$$

↳ In case of non magnetic dielect.

$$k = \frac{\omega}{v} = \frac{n\omega}{c}$$

$$k_1 = n_1 \omega / c \quad \& \quad k_2 = n_2 \omega / c$$

NOTE: Material with different permeability & permittivity

$$k_1 = \left(\frac{\omega}{c}\right) \sqrt{\mu_1 \epsilon_1}$$

$$k_2 = \left(\frac{\omega}{c}\right) \sqrt{\mu_2 \epsilon_2}$$

Eqn (\*\*\*) shows relation between  $\theta_I, \theta_R$  &  $\theta_T$

Now, Consider Boundary Condition requires Tangential Continuity of  $\vec{H}$  at  $(x=0)$   $\rightarrow$  all Negative  $y$ -direction (3)

$$H_{0I} + H_{0R} = H_{0T}$$

Using Eq<sup>n</sup>

$$E_{0I} \cos \theta_I e^{-jk_I z \sin \theta_I} + E_{0R} \cos \theta_R e^{jk_R z \sin \theta_R} = E_{0T} \cos \theta_T e^{-jk_T z \sin \theta_T}$$

$\therefore \theta_R = \theta_I$

So, we have

$$E_{0I} \cos \theta_I + E_{0R} \cos \theta_R = E_{0T} \cos \theta_T$$

$$E_{0I} \cos \theta_I + E_{0R} \cos \theta_2 = E_{0T} \cos \theta_2$$

$$\begin{aligned} \theta_I &\approx \theta_R = \theta_1 \\ \theta_T &= \theta_2 \end{aligned}$$

①

$$H_{0I} + H_{0R} = H_{0T}$$

$$\frac{E_{0I}}{\eta_1} - \frac{E_{0R}}{\eta_1} = \frac{E_{0T}}{\eta_2}$$

Intrinsic Impedance

$$\eta_1 = \frac{E_{0I}}{H_{0I}}$$

$$\eta_2 = \frac{E_{0T}}{H_{0T}}$$

②

Increase of refractive wave wense negative sign

Solve Eq<sup>n</sup> ① & ②

① + ②

$$\frac{1}{\eta_1} E_{0I} \cos \theta_I + \frac{1}{\eta_1} E_{0R} \cos \theta_I = \frac{1}{\eta_1} E_{0T} \cos \theta_2$$

$$\cos \theta_I \frac{E_{0I}}{\eta_1} - \frac{E_{0R}}{\eta_1} \cos \theta_I = \frac{E_{0T}}{\eta_2} \cos \theta_2$$

$$2 \cos \theta_I \frac{E_{0I}}{\eta_1} = E_{0T} \left( \frac{\cos \theta_2}{\eta_1} + \frac{\cos \theta_1}{\eta_2} \right)$$

$$\begin{aligned} (E_{0I} \cos \theta_1 + E_{0R} \cos \theta_2) \frac{1}{n_1} &= E_{0T} \cos \theta_2 \\ \left( \frac{E_{0I}}{n_1} - \frac{E_{0R}}{n_1} \right) \cos \theta_1 &= \frac{E_{0T}}{n_2} \cos \theta_2 \\ \hline 2 \cos \theta_1 \frac{E_{0R}}{n_1} &= E_{0T} \left( \frac{\cos \theta_2}{n_1} - \frac{\cos \theta_1}{n_2} \right) \end{aligned} \quad (4)$$

Take Ratio of (4) & (3)

$$\begin{aligned} \frac{E_{0R}}{E_{0I}} &= \frac{n_2 \cos \theta_2 - n_1 \cos \theta_1}{n_2 \cos \theta_2 + n_1 \cos \theta_1} = R(\bar{x}) = \Gamma_p \\ &= \frac{n_{2p} - n_{1p}}{n_{2p} + n_{1p}} \end{aligned} \quad \text{Reflection Coefficient}$$

Now from Eq<sup>n</sup> (1) & (2)

$$E_{0I} \cos \theta_1 + E_{0R} \cos \theta_1 = E_{0T} \cos \theta_2$$

$$\left( \therefore E_{0R} = E_{0I} - \frac{n_1}{n_2} E_{0T} \right) \text{ from Eq<sup>n</sup> (2)}$$

$$\therefore E_{0I} \cos \theta_1 + \left( E_{0I} - \frac{n_1}{n_2} E_{0T} \right) \cos \theta_1 = E_{0T} \cos \theta_2$$

$$2 E_{0I} \cos \theta_1 = E_{0T} \left[ \cos \theta_2 + \frac{n_1}{n_2} \cos \theta_1 \right]$$

$$= E_{0T} \left[ \frac{n_2 \cos \theta_2 + n_1 \cos \theta_1}{n_2} \right]$$

$$\therefore \frac{E_{0T}}{E_{0I}} = \frac{2 n_2 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2} \left( \frac{\cos \theta_2}{\cos \theta_1} \right)$$

$$\therefore \frac{E_{T0}}{E_{0I}} = \frac{2n_{2p}}{n_{2p} + n_{1p}} \left( \frac{\cos\theta_1}{\cos\theta_2} \right) = Z_p$$

Transmission Coefficient

where  $n_{2p} = n_2 \cos\theta_2$

$n_{1p} = n_1 \cos\theta_1$

For s-polarization (fig b)

Similarly we can write

$$\Gamma_s = \frac{E_{0R}}{E_{0I}} = \frac{n_{2s} - n_{1s}}{n_{2s} + n_{1s}}$$

$$T_s = \frac{E_{0T}}{E_{0I}} = \frac{2n_{2s}}{n_{2s} + n_{1s}}$$

Effective impedence for s-polarization are

$$n_{1s} = n_1 \sec\theta_1$$

$$n_{2s} = n_2 \sec\theta_2$$

## Total Internal Reflection:-

When light strikes an Angle of incidence greater than critical Angle,

- All the light energy will be reflected back
- None of them will be absorbed.

Critical Angle is related to the refractive index of the two media is given by

$$\theta_c = \sin^{-1} \left( \frac{n_2}{n_1} \right)$$

From Snell's second law,

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$\theta_i$  = incident Angle

$$\sin \theta_i = \frac{n_2}{n_1} \sin \theta_t$$

$\theta_t$  = Transmitted angle

Case: I If  $\theta_i = \theta_c$ ,  $\theta_t = \frac{\pi}{2}$

If we consider non-magnetic material

( $\mu_1 = \mu_2 = 1$ )

$$\sin \theta_i = \frac{\sqrt{\epsilon_2} \sin \theta_t}{\sqrt{\epsilon_1}}$$

$$\sin \theta_c = \frac{\sqrt{\epsilon_2} \sin \frac{\pi}{2}}{\sqrt{\epsilon_1}} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}}$$

$$\theta_c = \sin^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right)$$

$$= \sin^{-1} \left( \sqrt{\frac{\mu_0 \mu_{r2} \epsilon_0 \epsilon_{r2}}{\mu_0 \mu_{r1} \epsilon_0 \epsilon_{r1}}} \right)$$

$$= \sin^{-1} \left( \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{\mu_{r1} \epsilon_{r1}}} \right) = \sin^{-1} \left( \frac{n_2}{n_1} \right)$$

Case II  $\theta_i > \theta_c$

For dielectric medium

$$\mu_{r1} = \mu_{r2} = 1, \quad \epsilon_1 > \epsilon_2$$

$$\sin \theta_t = \frac{\sqrt{\mu_1 \epsilon_1}}{\sqrt{\mu_2 \epsilon_2}} \sin \theta_i > 1$$

$$\cos \theta_t = \pm \sqrt{1 - \sin^2 \theta_t} \quad \cos \theta_t \text{ should be Imaginary}$$

NOW,

$$\vec{S} = \vec{E} \times \vec{H}$$

$$= \frac{|E_0|^2}{n_2} e^{-jz k_2 \cos \theta_t} \sin \theta_t \hat{x} + \hat{z} \frac{|E_0|^2}{n_2} e^{-jz k_2 \cos \theta_t} \cos \theta_t$$

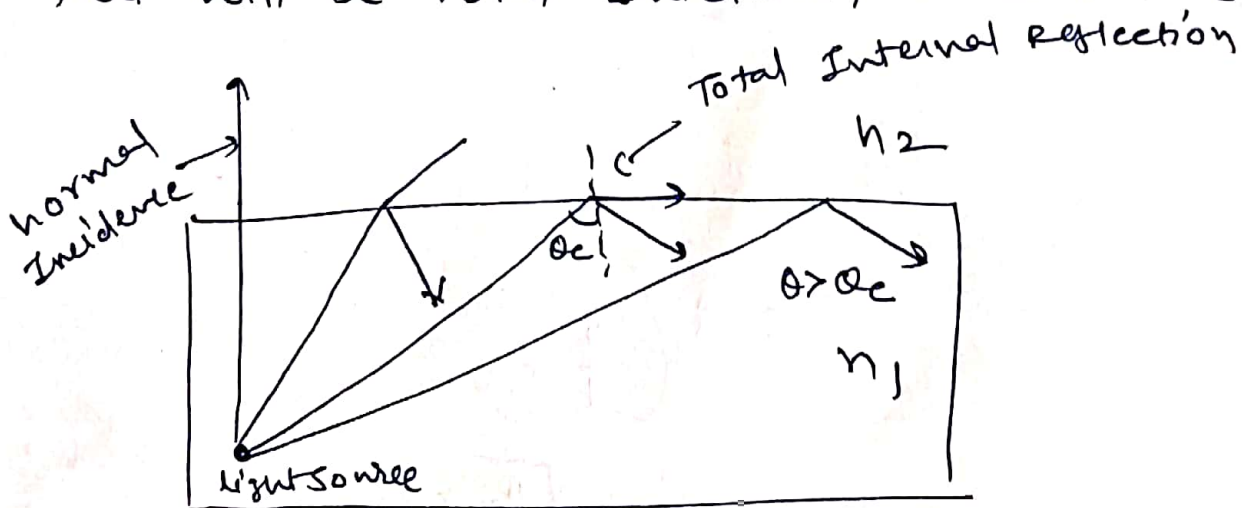
For  $z > 0$ ,  $\cos \theta_t$  is Imaginary Number  
 $\cos \theta_t^*$  is purely Imaginary

So, second term is Imaginary, No real power is flowing along z-axis in Region II

— First term has direction along x-axis & real & is Exponentially decaying

— Hence, when  $\theta_i > \theta_c$  from Region I

that will be total Internally reflected in Region I



Example: -

If  $\eta_1 = 100 \Omega$ ,  $\eta_2 = 300 \Omega$ ,  $E_{in} = 100 \text{ V/m}$   
then calculate values for the incident, reflected  
& transmitted waves

→ Reflection coefficient at normal incidence  
is given by

$$\frac{E_R}{E_I} = \Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{300 - 100}{300 + 100} = 0.5$$

$$E_{Ref} = \left( \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \right) E_I$$

$$\therefore E_{Ref} = 0.5 \times 100 = 50 \text{ V/m}$$

Transmission coefficient

$$\tau = \frac{2\eta_2}{\eta_2 + \eta_1} = \frac{E_T}{E_I}$$

$$\tau = \frac{2 \times 300}{300 + 100} = \frac{600}{400} = \frac{3}{2}$$

$$E_T = \frac{3}{2} \times 100 = 150 \text{ V/m}$$

Electric Intensities are:  $E_I = 100 \text{ V/m}$   $E_T = 150 \text{ V/m}$   
 $E_R = 50 \text{ V/m}$

→ For magnetic intensity

$$H_I = \frac{E_I}{\eta_1} = \frac{100}{100} = 1 \text{ A/m}$$

$$H_T = \frac{E_T}{\eta_2} = \frac{150}{300} = 0.5 \text{ A/m}$$

$$H_R = \frac{E_R}{\eta_1} = \frac{50}{100} = 0.5 \text{ A/m}$$



A uniform plane wave is incident from air onto glass at an angle from the normal of  $30^\circ$ . determine the fraction of the incident power that is reflected & transmitted <sup>coefficient</sup> for (a) p-polarization (b) s-polarization. Glass has refractive index  $n_2 = 1.45$   
 $n_1 = 1$  (air)

→  $n_1 \sin \theta_1 = n_2 \sin \theta_2$  (refractive index)

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1 = \frac{1}{1.45} \sin 30^\circ$$

$$= \frac{1.45}{1} \sin 30^\circ \quad \theta_2 = \sin^{-1} \left( \frac{\sin 30^\circ}{1.45} \right) = 20.2^\circ$$

P-polarization

$$\because \eta_1 = \frac{\eta_0}{n_1} \rightarrow (377)$$

$$\eta_{1p} = \eta_1 \cos \theta_1 = 377 \cos(30^\circ) = 326 \Omega$$

$$\eta_{2p} = \eta_2 \cos \theta_2 = \frac{377}{1.45} \cos 20.2^\circ = 244 \Omega$$

↓  
Impedance

$$\Gamma_p = \frac{244 - 326}{244 + 326} = -0.144$$

$$\tau_p = \frac{2\eta_{2p}}{\eta_{1p} + \eta_{2p}} = \frac{244}{244 + 326}$$

S-polarization,

$$\eta_{1s} = \eta_1 \sec 30^\circ = 377 (1.1547) = 435 \Omega$$

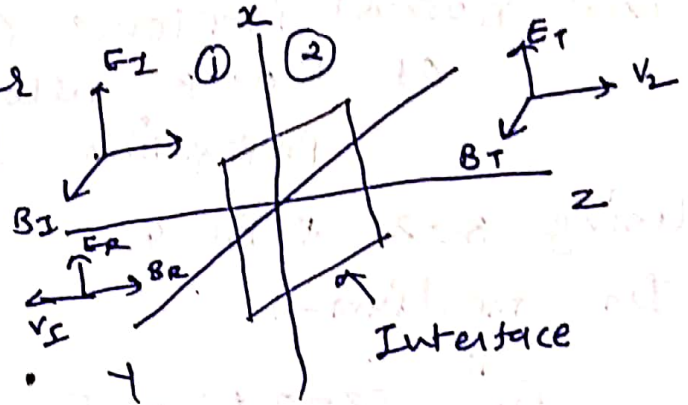
$$\eta_{2s} = \eta_2 \sec 20.2^\circ = 277 \Omega$$

$$\Gamma_s = \frac{\eta_{2s} - \eta_{1s}}{\eta_{2s} + \eta_{1s}} = -0.222$$

$$\tau_s = \frac{2\eta_{2s}}{\eta_{2s} + \eta_{1s}} = \frac{2 \times 277}{277 + 435}$$

(\*) Reflection and Transmission of plane waves at normal incidence:

x-y Plane Boundary  
between two linear media  
plane wave travelling  
in z-direction



Incident EM wave

Propagates in +z direction

$$E_{in} = E_{0I} e^{i(k_1 z - \omega t)} \hat{x}$$

$$B_{in} = \frac{1}{v_1} k_1 \times E_I = \frac{1}{v_1} E_{0I} e^{i(k_1 z - \omega t)} \hat{y}$$

Reflected EM wave

Propagates in -z direction

$$E_R = E_{0R} e^{i(k_1 z - \omega t)} \hat{x}$$

$$B_R = \frac{1}{v_1} k_R \times E_R = -\frac{1}{v_1} E_{0R} e^{i(-k_1 z - \omega t)} \hat{y}$$

Transmitted EM wave

Propagates in +z direction

$$E_T = E_{0T} e^{i(k_2 z - \omega t)} \hat{x}$$

$$B_T = \frac{1}{v_2} k_T \times E_T = \frac{1}{v_2} E_{0T} e^{i(k_2 z - \omega t)} \hat{y}$$

Boundary Conditions:

BC1: Normal  $\vec{D}$  continuous

$$\epsilon_1 E_{1 \perp \text{Tot}} = \epsilon_2 E_{2 \perp \text{Tot}} \quad (\text{in z direction})$$

(x-y Boundary)

BC2: Tangential  $\vec{E}$  continuous

$$E_{1 \parallel \text{Tot}} = E_{2 \parallel \text{Tot}}$$

BC 3

Normal  $\bar{B}$  continuous:  $B_{1\text{Tot}}^\perp = B_{2\text{Tot}}^\perp$

BC 4

Tangential  $\bar{E}$  Continuous:  $\frac{1}{\mu_1} B_{1\text{Tot}}^\parallel = \frac{1}{\mu_2} B_{2\text{Tot}}^\parallel$

For normal incidence ( $z=0$ ) - no components of  $\bar{E}$  or  $\bar{B}$  allowed to be along  $\pm z$  propagation direction,

Using BC-2 & BC-4

In medium-1.

$$E_{1\text{Tot}}^\parallel(z=0, t) = E_{\text{inc}}^\parallel(z=0, t) + E_r^\parallel(z=0, t)$$

$$\frac{1}{\mu_1} B_{1\text{Tot}}^\parallel(z=0, t) = \frac{1}{\mu_1} B_I^\parallel(z=0, t) + \frac{1}{\mu_1} B_R^\parallel(z=0, t)$$

In medium-2

$$E_{1\text{Tot}}^\parallel(z=0, t) = E_T^\parallel(z=0, t)$$

$$\frac{1}{\mu_2} B_{2\text{Tot}}^\parallel(z=0, t) = \frac{1}{\mu_2} B_{T\text{Tot}}^\parallel(z=0, t)$$

Using BC2

$$E_{1\text{Tot}}^\parallel = E_{2\text{Tot}}^\parallel$$

$$\therefore E_I \neq E_R \neq E_T$$

$$\therefore E_{0I} e^{-i\omega t} \neq E_{0R} e^{-i\omega t} = E_{0T} e^{-i\omega t}$$

$$\therefore E_{0I} + E_{0R} = E_{0T}$$

— (1)

Using BC-4

$$\frac{1}{\mu_1} B_{1\text{Tot}}^\parallel = \frac{1}{\mu_2} B_{2\text{Tot}}^\parallel$$

$$\frac{1}{\mu_1} B_I + \frac{1}{\mu_1} B_R = \frac{1}{\mu_2} B_T$$

$$\frac{1}{\mu_1 \nu_1} E_{0I} e^{-i\omega t} - \frac{1}{\mu_1 \nu_1} E_{0R} e^{-i\omega t}$$

$$= \frac{1}{\mu_2 \nu_2} E_{0T} e^{-i\omega t}$$

$$\frac{1}{\mu_1 \nu_1} E_{0I} - \frac{1}{\mu_1 \nu_1} E_{0R} =$$

$$\frac{1}{\mu_2 \nu_2} E_{0T}$$

$$\frac{1}{\mu_1 \nu_1} (E_{0I} - E_{0R}) = \frac{1}{\mu_2 \nu_2} E_{0T}$$

Now,  $E_{o1} - E_{o2} = \frac{\mu_1 v_1}{\mu_2 v_2} E_{oT}$

$E_{o1} - E_{o2} = \beta E_{oT}$  — (3)

$(\because \frac{\mu_1 v_1}{\mu_2 v_2} = \beta)$

Eq<sup>n</sup> (1) + Eq<sup>n</sup> (3)

$E_{o1} + E_{o2} = E_{oT}$   
 $E_{o1} - E_{o2} = \beta E_{oT}$

$2E_{o1} = (1 + \beta)E_{oT}$

$E_{oT} = \left(\frac{2}{1 + \beta}\right)E_{o1}$  — (4)

Eq<sup>n</sup> (1) - Eq<sup>n</sup> (3)

$E_{o1} + E_{o2} = E_{oT}$   
 $E_{o1} - E_{o2} = \beta E_{oT}$

$2E_{o2} = (1 - \beta)E_{oT}$

$E_{o2} = \left(\frac{1 - \beta}{2}\right)E_{oT}$  — (5)

Put Eq<sup>n</sup> (4)  $\rightarrow$  Eq<sup>n</sup> (5)

$E_{o2} = \left(\frac{1 - \beta}{2}\right) \left(\frac{2}{1 + \beta}\right) E_{o1}$

$E_{o2} = \left(\frac{1 - \beta}{1 + \beta}\right) E_{o1}$

As we know,

$\beta = \frac{\mu_1 v_1}{\mu_2 v_2}$

$v_1 = \frac{c}{n_1}, v_2 = \frac{c}{n_2}$

$n_1 = \sqrt{\frac{\epsilon_1 \mu_1}{\epsilon_0 \mu_0}}$

$n_2 = \sqrt{\frac{\epsilon_2 \mu_2}{\epsilon_0 \mu_0}}$

$\beta = \frac{\mu_1 (c/n_1)}{\mu_2 (c/n_2)} = \frac{\mu_1 n_2}{\mu_2 n_1}$

$\beta = \frac{\mu_1 \sqrt{\epsilon_2 \mu_2 / \epsilon_0 \mu_0}}{\mu_2 \sqrt{\epsilon_1 \mu_1 / \epsilon_0 \mu_0}}$   
 $= \sqrt{\frac{\epsilon_2 \mu_1}{\epsilon_1 \mu_2}}$

If two media are both paramagnetic or diamagnetic

$$|X_{m1,2}| \ll 1$$

$$\mu_1 = \mu_0(1 + X_{m1}) \approx \mu_0, \quad \mu_2 = \mu_0(1 + X_{m2}) \approx \mu_0$$

$$\text{So, } \beta = \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{v_1}{v_2} = \frac{n_2}{n_1}$$

So, now we have

$$E_{0R} = \left( \frac{1 - \beta}{1 + \beta} \right) E_{0I} = \left( \frac{1 - (v_1/v_2)}{1 + (v_1/v_2)} \right) E_{0I}$$

$$E_{0R} = \left( \frac{v_2 - v_1}{v_2 + v_1} \right) E_{0I}$$

$$E_{0T} = \left( \frac{2}{1 + \beta} \right) E_{0I} = \left( \frac{2}{1 + (v_2/v_1)} \right) E_{0I}$$

$$E_{0T} = \left( \frac{2v_2}{v_1 + v_2} \right) E_{0I}$$

Reflection Coefficient

$$R = \frac{E_{0R}}{E_{0I}}$$

$$= \frac{v_2 - v_1}{v_2 + v_1}$$

$$= \frac{n_1 - n_2}{n_1 + n_2}$$

Transmission Coefficient

$$T = \frac{E_{0T}}{E_{0I}}$$

$$= \frac{2v_2}{v_1 + v_2}$$

$$= \frac{2n_1}{n_1 + n_2}$$